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# Electronic Instrumentation

## Chapter 2

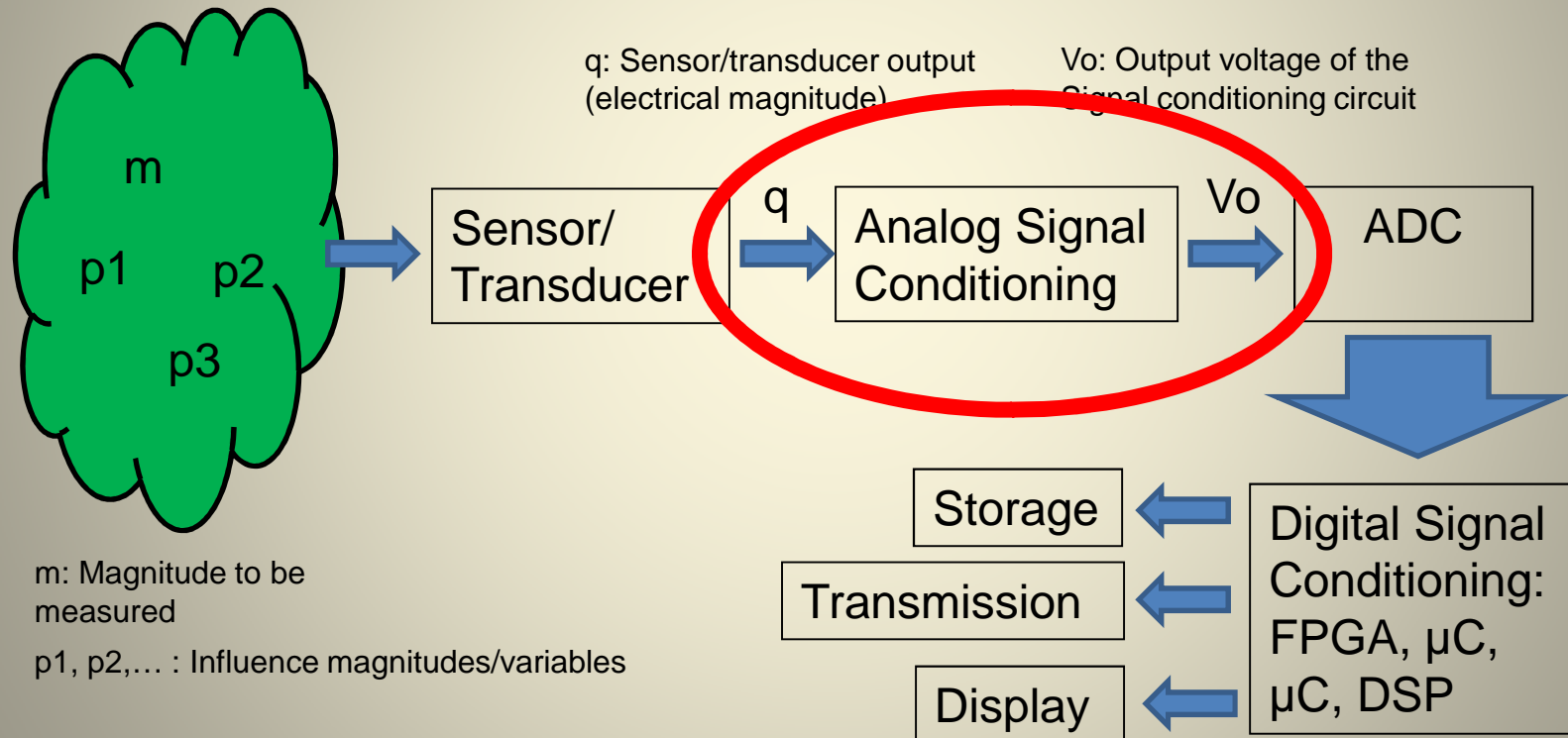
### Analog Signal Conditioning



# Chapter 2. Signal Conditioning

- Introduction
- Passive Sensors Conditioning
- DC Null Measurements
- AC Null Measurements
- Instrumentation Amplifiers
- Linear and Nonlinear Analog Signal Processing and Special Function Modules
- Other specific Instrumentation Components and circuits

# Basic Architecture for an Electronic Instrumentation Measurement System





# Introduction to Analog Signal Conditioning

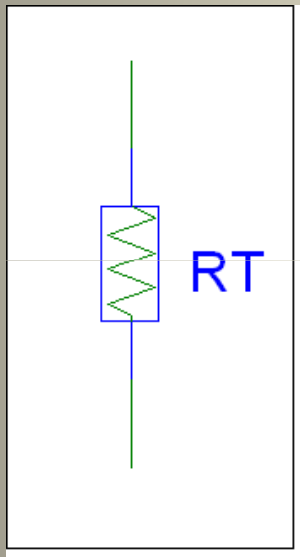
- Convert the changes of an impedance  $Z$  into an electric output that is easily processed (voltage).
- Minimize the non-linear error of the primary output and the overall output.
- Compensate magnitudes of influence (sources of errors).
- Enhance the sensitivity (amplification).
- Adjust the signal levels (range, zero, etc.).
- Other practical issues: isolation, etc.
- Linear filtering (analog filters and integrators).
- In some cases, nonlinear processing: RMS, Log, phase-sensitive demodulators.



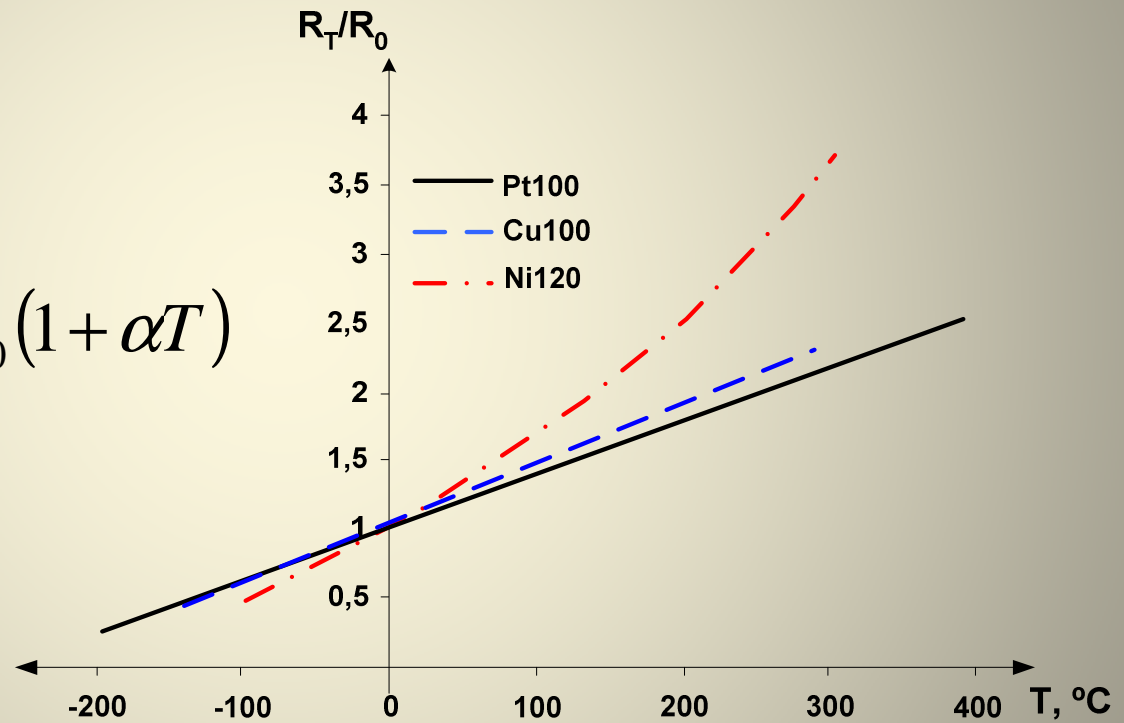
# Need of passive sensors conditioning

- Conversion of the changes of an impedance  $Z$  into an electric output that is easily processed (voltage  $V_m$ )
- NOTE: Sensitivity depends on the voltage reference  $V_{cc}$
- Sensitivity is greater with more  $V_{cc}$ , but the limits to the voltage reference  $V_{cc}$  are:
  - Maximum power dissipation limits the sensitivity ( $V_{cc}$  max)
  - Self-heating of the sensor due to power dissipation introduce a source of error
- Impedance not only reduce the sensitivity, but also introduce non-linearity error due to sensitivity changes.
- Amplification completes the analog conditioning (adjustment of Gain and Zero, and high input impedance)

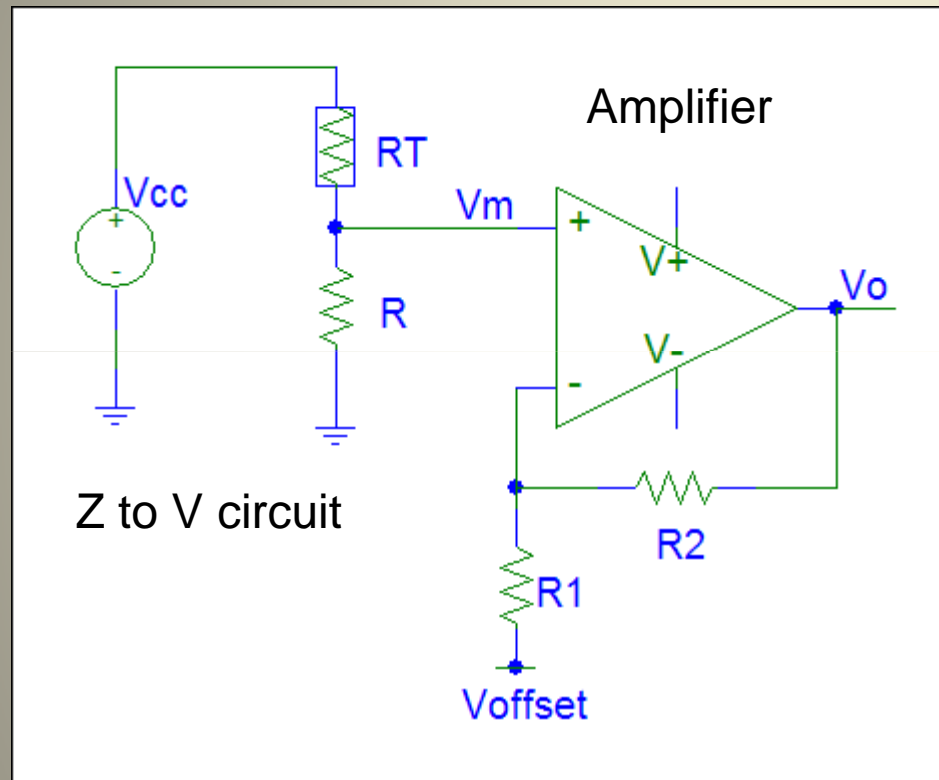
# Passive sensor: Example



$$R_T = R_0(1 + \alpha T)$$



# Basic passive sensors conditioning circuits

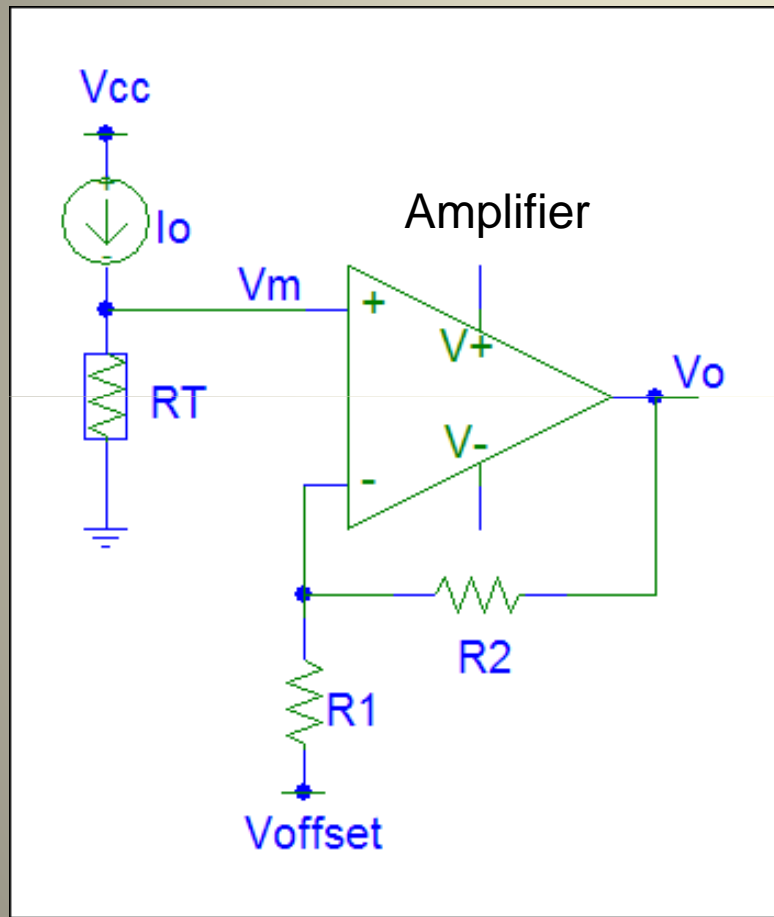


Amplifier with very high  
input impedance  $Z_i$ , very  
low output impedance  $Z_o$

$$V_m = V_{cc} \frac{R}{R + R_T}$$

$$V_o = V_m \frac{R_1 + R_2}{R_1} - V_{offset} \frac{R_2}{R_1}$$

# Basic passive sensors conditioning circuits



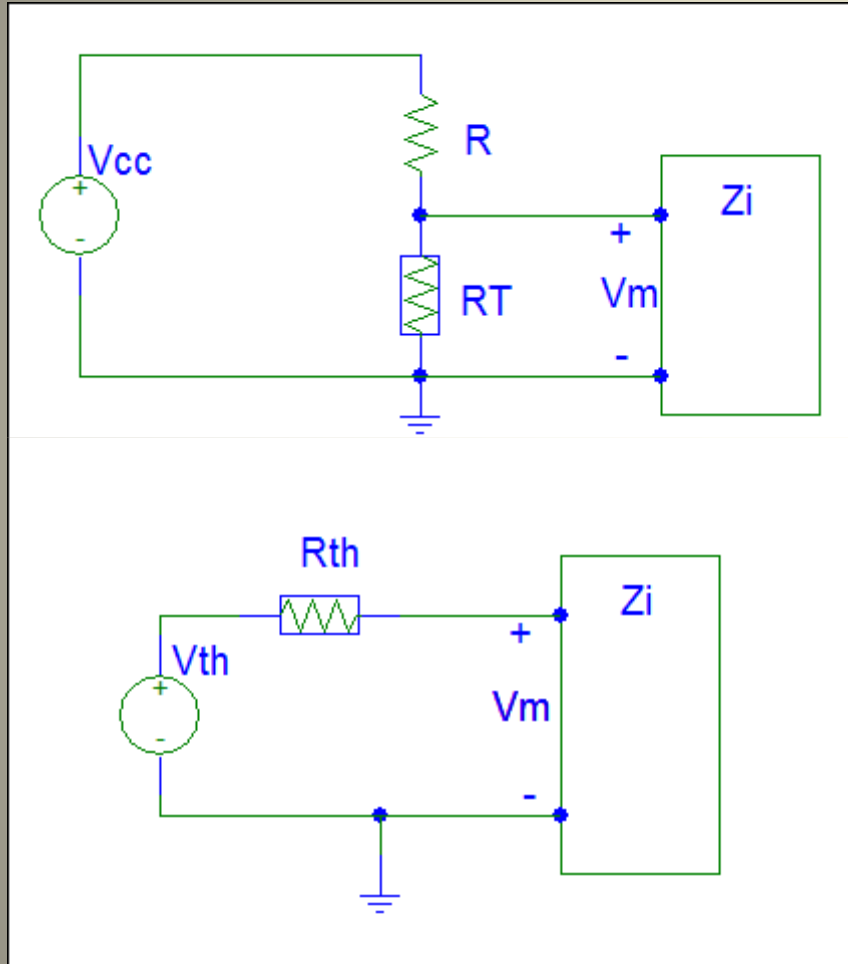
$$V_m = I_o \cdot R_T$$

Good linearity over a wide range

$$V_o = V_m \frac{R_1 + R_2}{R_1} - V_{offset} \frac{R_2}{R_1}$$



## Potentiometric circuit (a case study)



$$V_m = f(m, p_1, p_2, \dots)$$

Equations:

$$V_m = V_{CC} \frac{R_T}{R + R_T}$$

$$R_T(m) = R_0 + \Delta R_m = R_0 + S_m \cdot m$$

$$R_T(m, i) = R_0 + S_m \cdot m + S_i \cdot i$$

Questions:

- Load effect  $R_{th}$
- Linearity
- Maximum sensitivity ( $R=R_0$ )
- Magnitudes of influence
- $V_m$  not null if  $m=0$  !!!

# Potentiometric circuit (a case study)

Sensitivity

$$S = \frac{\partial V_m}{\partial m} = S_m \cdot V_{CC} \frac{R}{(R + R_T)^2}$$

Maximum sensitivity

$$S_{\max} \Leftrightarrow \frac{\partial S}{\partial R} = 0 \Rightarrow R = R_0$$

Effect of magnitudes of influence

$$\frac{\partial V_m}{\partial i} = S_i \cdot V_{CC} \frac{R}{(R + R_T)^2}$$

Compensation of magnitudes of influence

$$\frac{\partial V_m}{\partial i} = 0$$

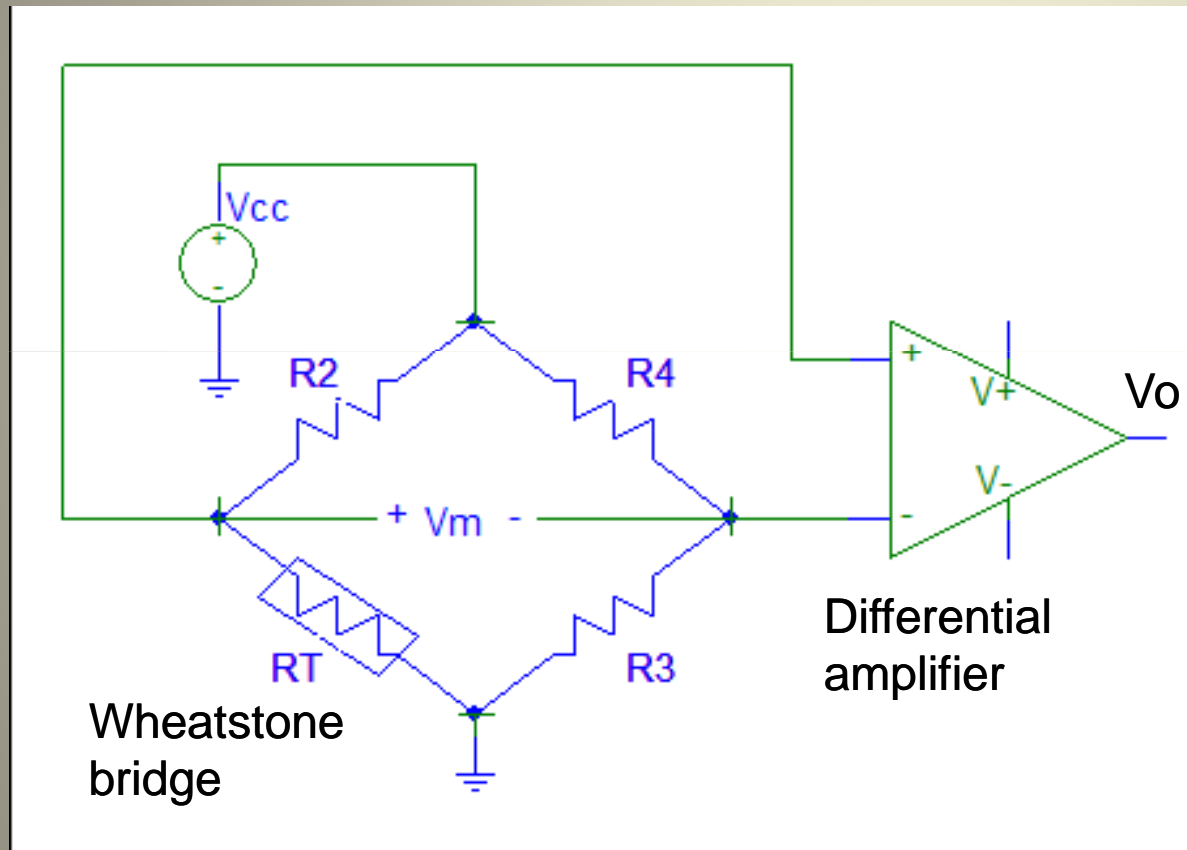
$$V_m = V_{CC} \frac{R_T}{R + R_T}$$

$$R_T(m) = R_0 + S_m \cdot m$$

$$R_T(m, i) = R_0 + S_m \cdot m + S_i \cdot i$$

$$R(i) = R_0 + S_i \cdot i$$

# DC Null Measurements



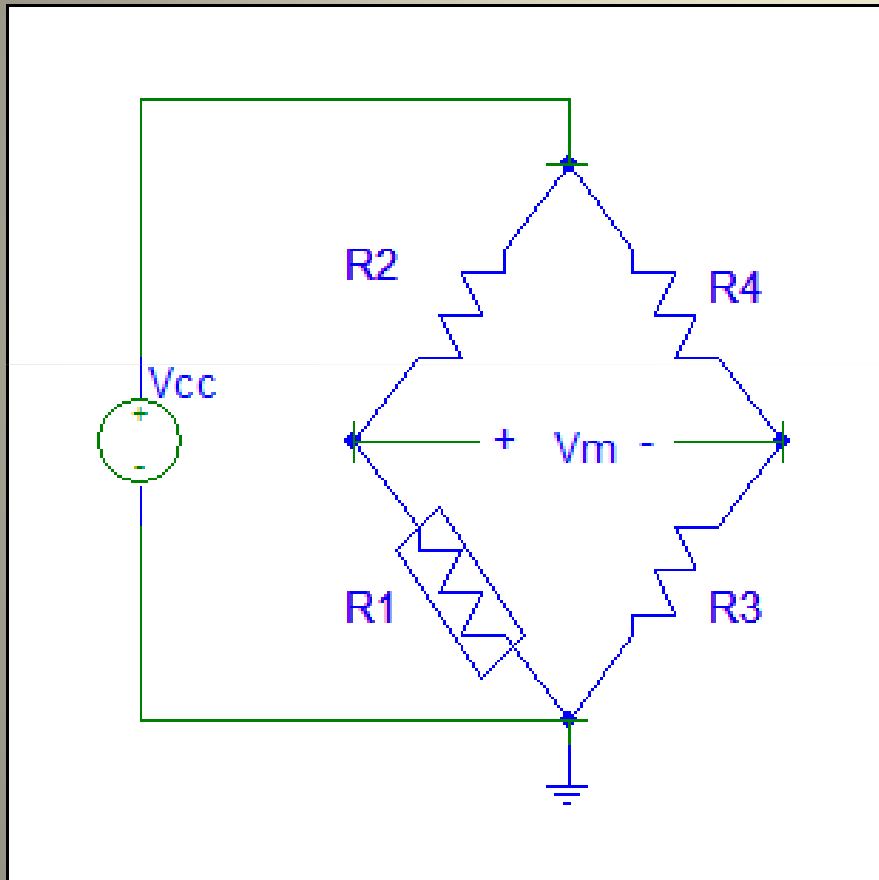
Output  $V_o$  is null if  $m = 0$

Better detection of low magnitudes around zero

Differential amplification and high Common Mode Rejection Ratio (CMRR)

Loading of differential amplifier input impedance

# Wheatstone bridge



Equations:

$$V_m = V_{cc} \left[ \frac{R_1}{R_1 + R_2} - \frac{R_3}{R_3 + R_4} \right]$$

Equilibrium ( $V_m = 0$ ):

$$R_1 \cdot R_4 = R_2 \cdot R_3$$

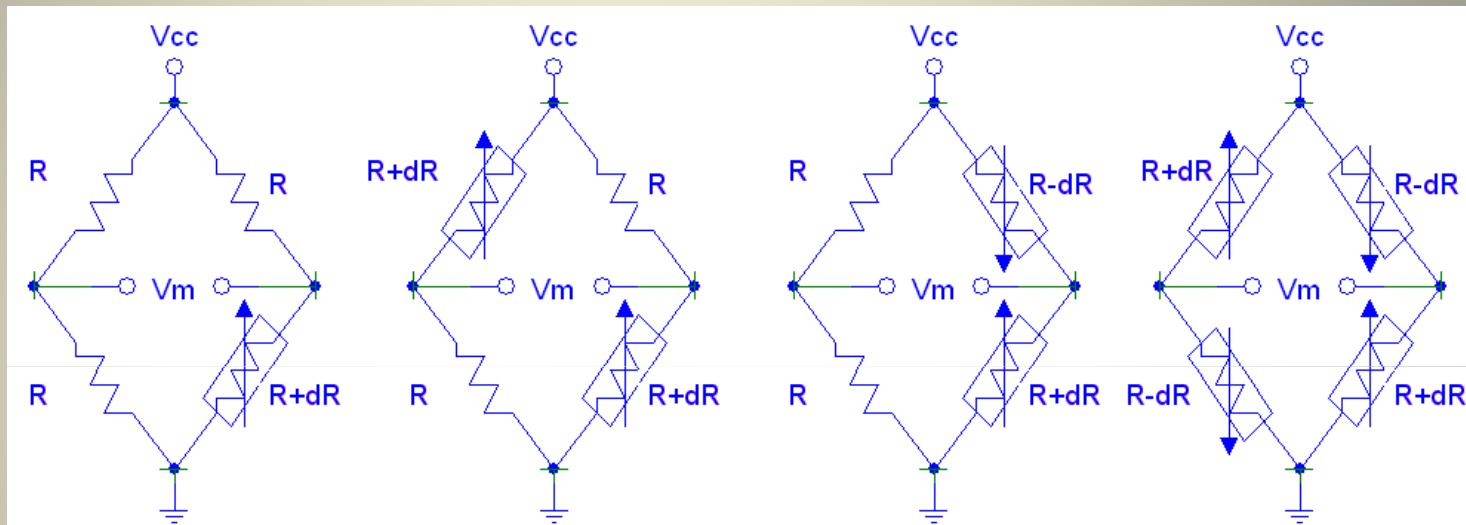
Maximum sensitivity:

$$R_1(m) = R_0 + \Delta R_m = R_0 + S_m \cdot m$$

$$R_2 = R_0 \quad \text{and} \quad R_3 = R_4$$

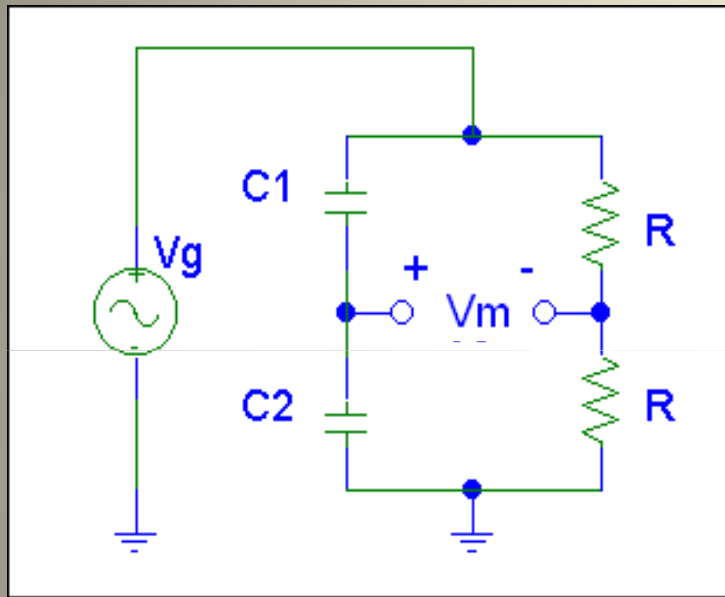
$$V_m = V_{cc} \left[ \frac{R_0 + \Delta R_m}{2R_0 + \Delta R_m} - \frac{1}{2} \right] = V_{cc} \left[ \frac{\Delta R_m}{4R_0 + 2\Delta R_m} \right]$$

# Wheatstone bridge sensitivity, linearity, push-pull and errors due to magnitudes of influence

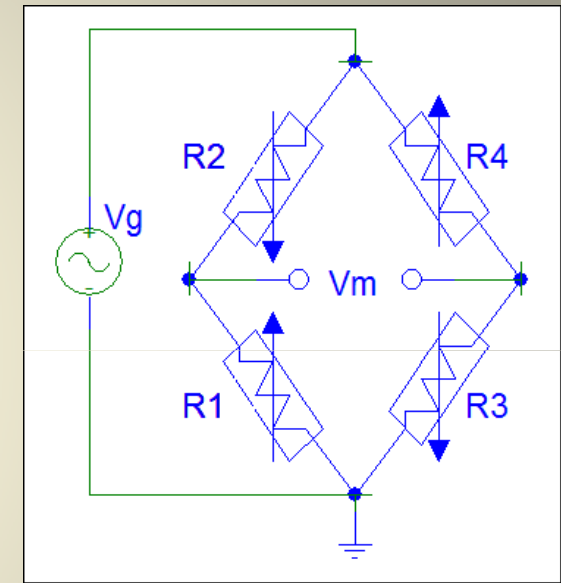
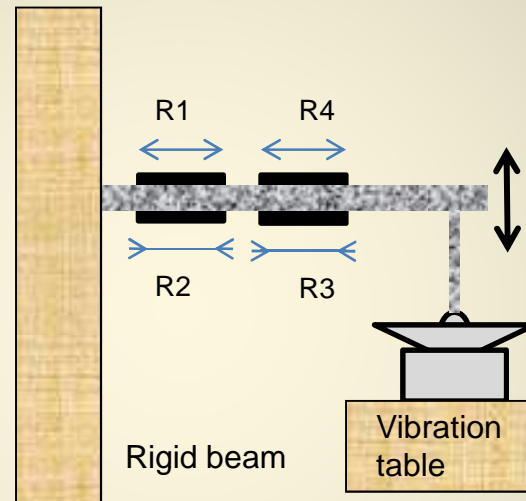


<b>V<sub>m</sub></b>	$\frac{V_{cc}}{4} \left[ \frac{\Delta R}{R_o + \frac{\Delta R}{2}} \right]$	$\frac{V_{cc}}{2} \left[ \frac{\Delta R}{R_o + \frac{\Delta R}{2}} \right]$	$\frac{V_{cc}}{2} \left[ \frac{\Delta R}{R_o} \right]$	$V_{cc} \left[ \frac{\Delta R}{R_o} \right]$
<b>Linearity Error</b>	0.5%/%	0.5%/%	0	0
	A) Single-Element varying	B) Two-Element varying (1)	C) Two-Element varying (2) Push-pull	D) All-Element varying

# Need of AC Null Measurements

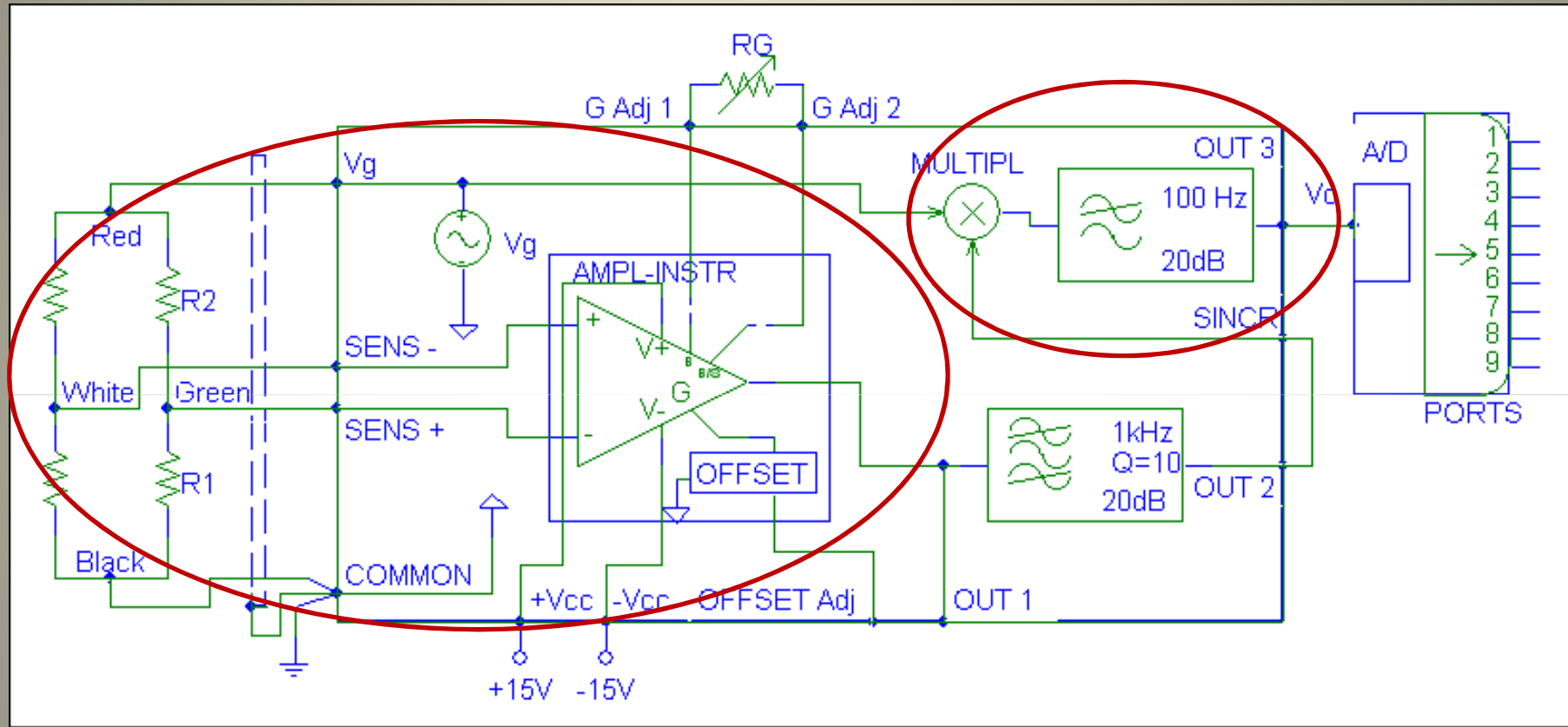


Analog conditioning of  
Capacitive and inductive sensors  
(complex impedances)



$V_g$  is the carrier of the  
modulated electronic system  
(reference oscillator)

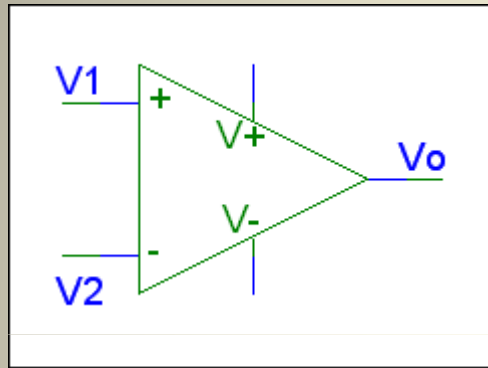
# Demodulation in AC Null Measurements



Vg Carrier  
Wheatstone bridge configuration  
Instrumentation amplifier (differential)

Band-pass filters  
Multiplier and Low-pass filter  
or Synchronous demodulator

# Differential amplifiers



Differential input

$$V_m = V_1 - V_2$$

Common mode input

$$V_c = \frac{V_1 + V_2}{2}$$

General

$$V_o = A \cdot V_1 + B \cdot V_2$$

Differential mode gain  
and Common mode gain

$$V_o = A_{DM} \cdot V_m + A_{CM} \cdot V_c$$

Common Mode  
Rejection Ratio

$$V_o = A_{DM} \left( V_m + \frac{V_c}{CMRR} \right)$$

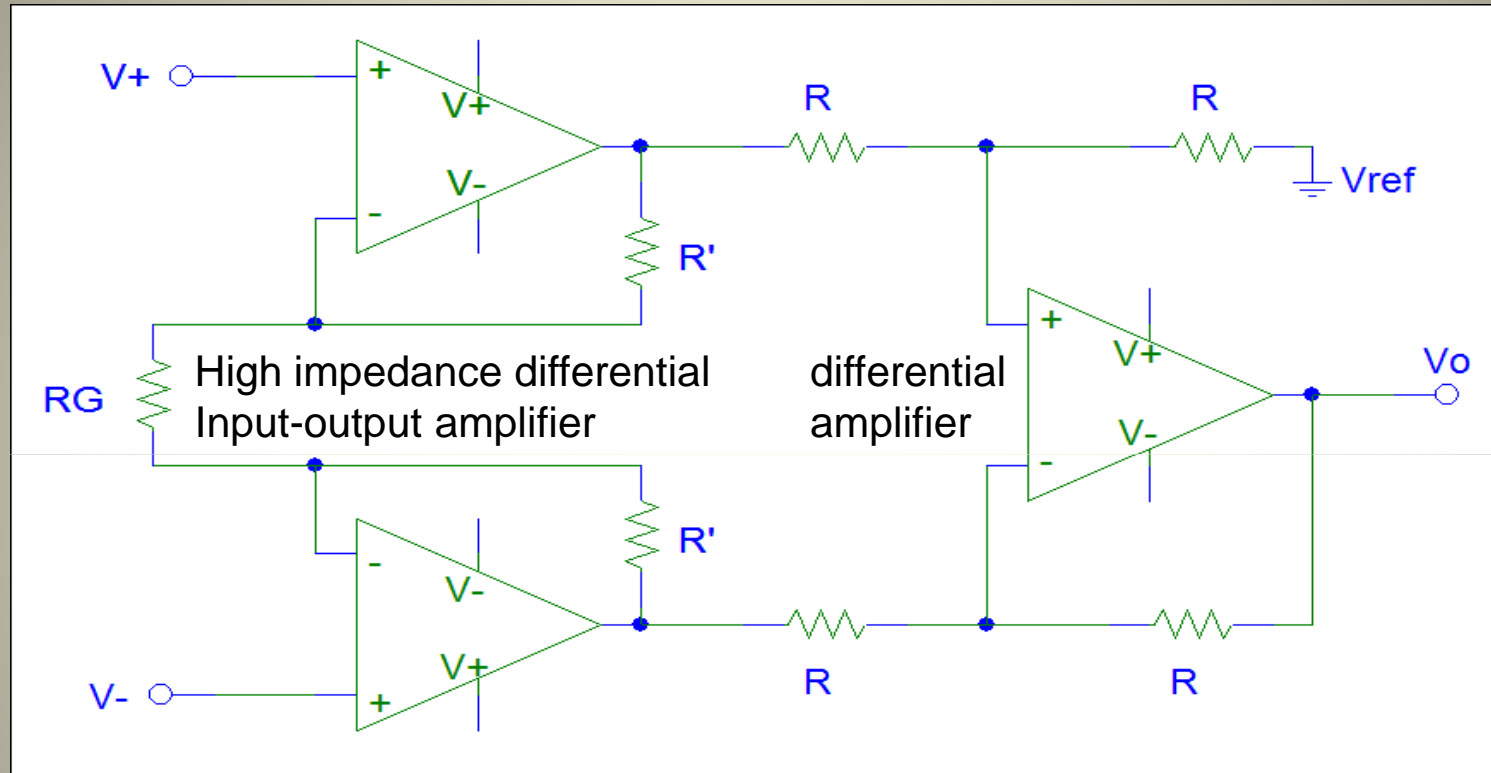




# Need of instrumentation amplifiers

- High differential gain
- High CMRR (common mode rejection ratio)
- High input impedance minimize loading effects maximizing the overall sensitivity and avoiding non-linearity error due to sensitivity changes
- Easy adjustment of the gain with a simple passive component
- Integrated circuit for a trim adjustment of the parameters

# Structure of instrumentation amplifiers



$$v_o = \frac{R}{R} \cdot \left( 1 + \frac{2R'}{R_G} \right) (v_+ - v_-)$$

RG selects Gain

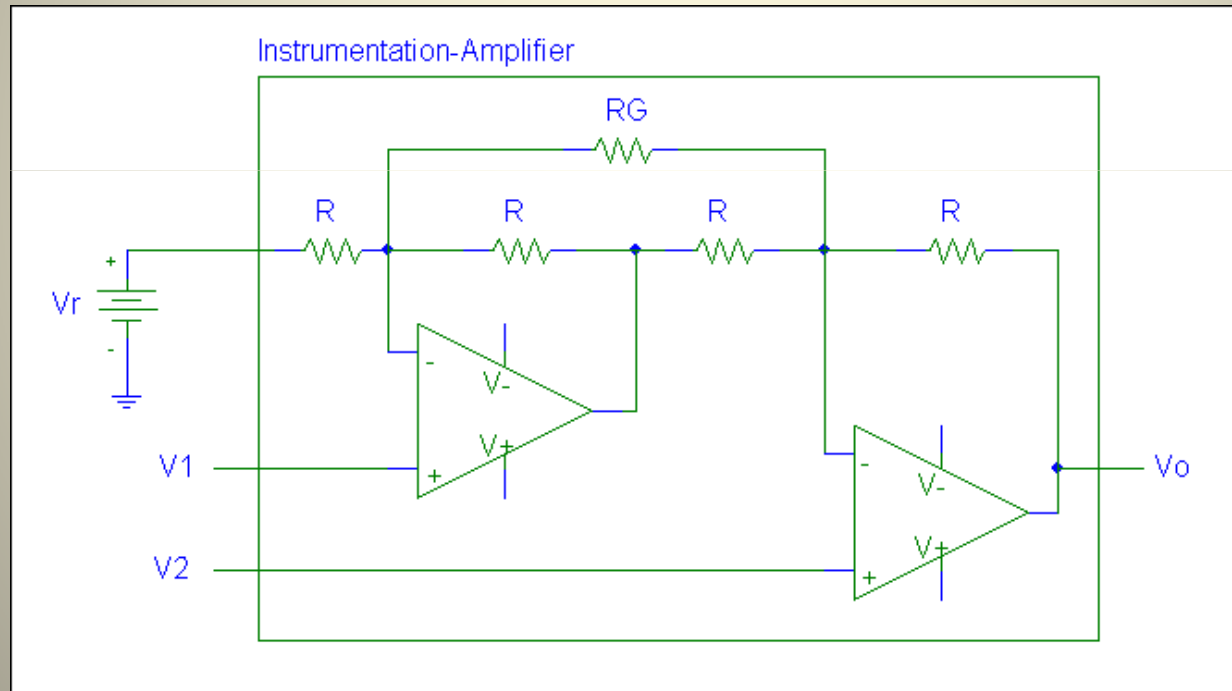
Trimmed R values

# Integrated instrumentation amplifiers

\* AD620

\* Others

Two OA instrumentation amplifier

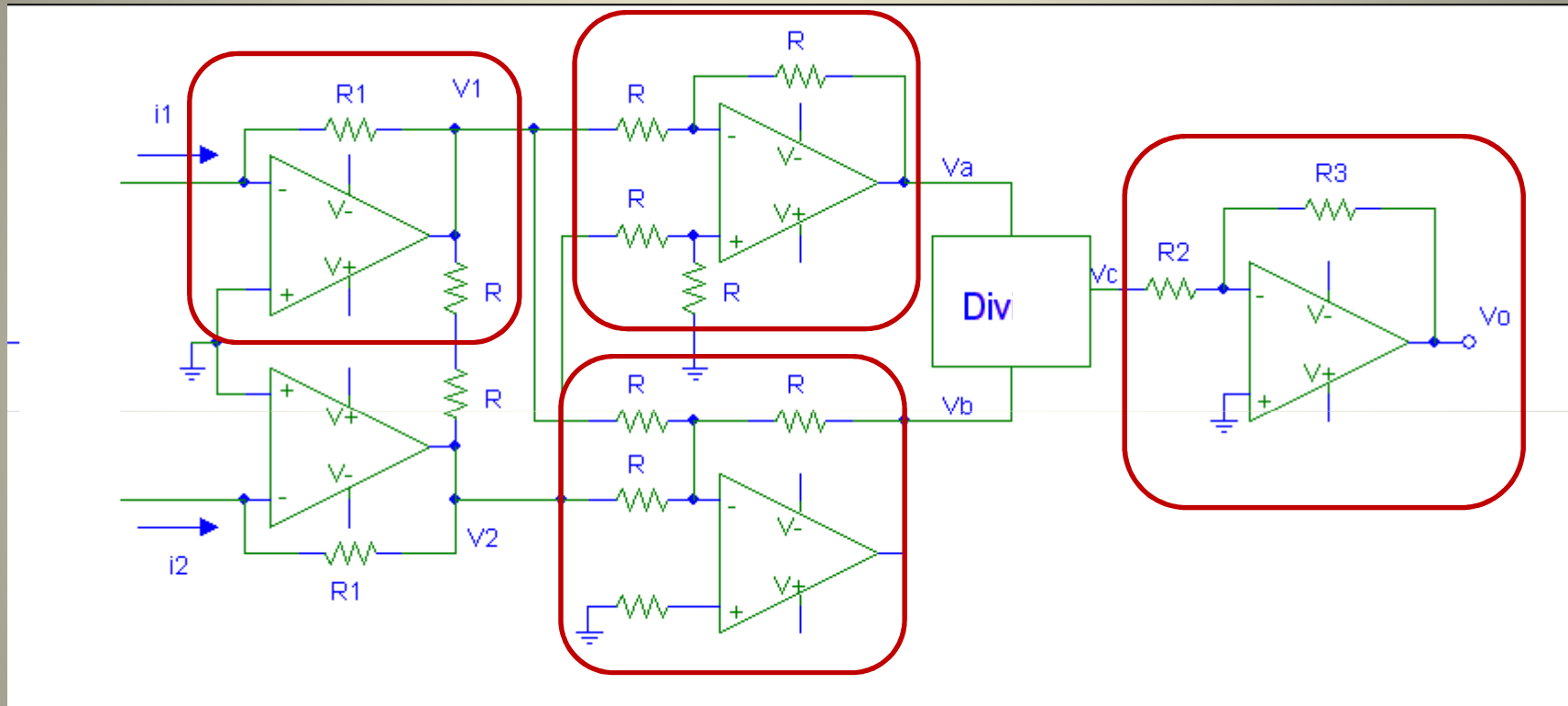




# Basic linear analog signal processing

- Operational Amplifiers are used in a circuit as a negative feedback amplifier
- Types of Operational Amplifiers
- Survey of applications
  - Inverting, non-inverting, adding and differential amplifiers
  - Current to voltage and voltage to current conversions
  - Integrators and differentiators
  - Analog active filters

# Example of signal conditioning with OA

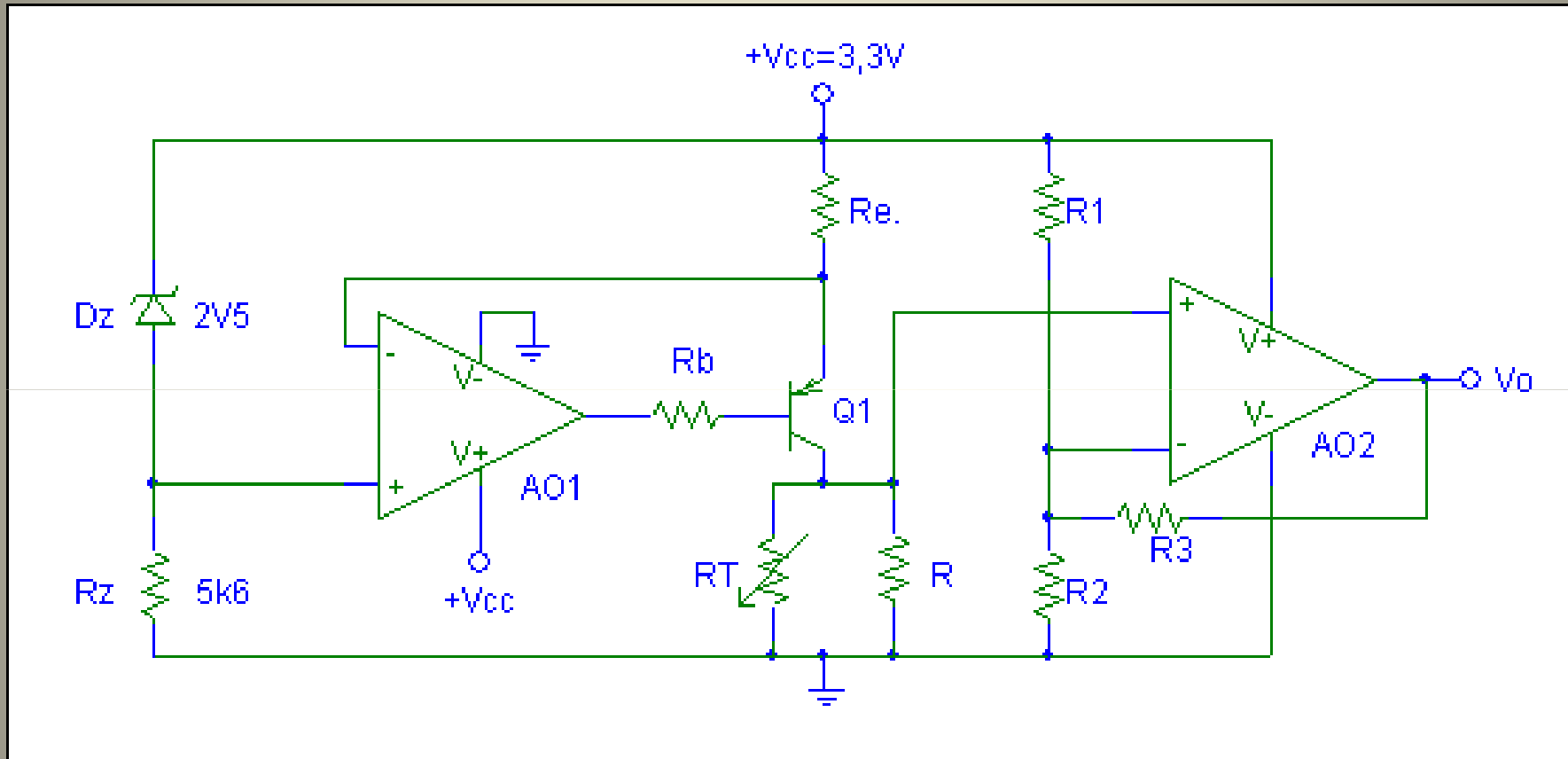


Current to voltage  
amplifiers

Differential amplifier and  
Adding amplifiers

Inverting amplifier  
(recommended)

# Example of signal conditioning with OA



Voltage to current amplifier  
or current source

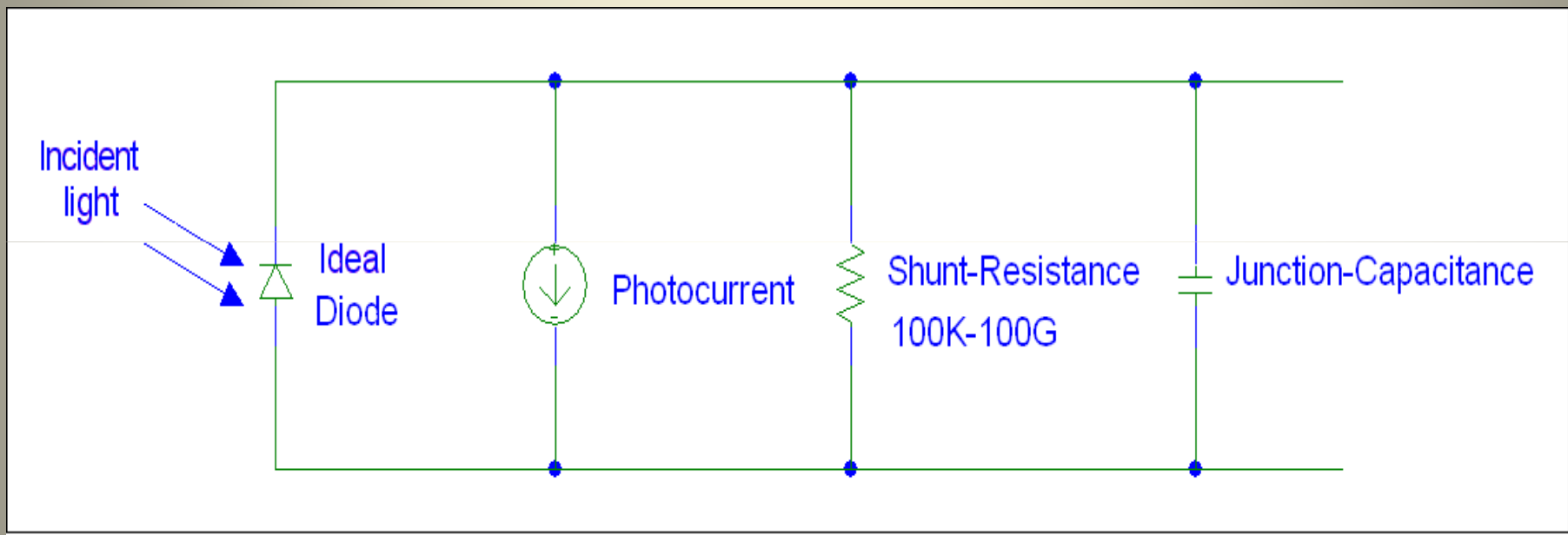
Amplifier with gain and zero  
adjustment



## Analog signal conditioning of optoelectronic sensors

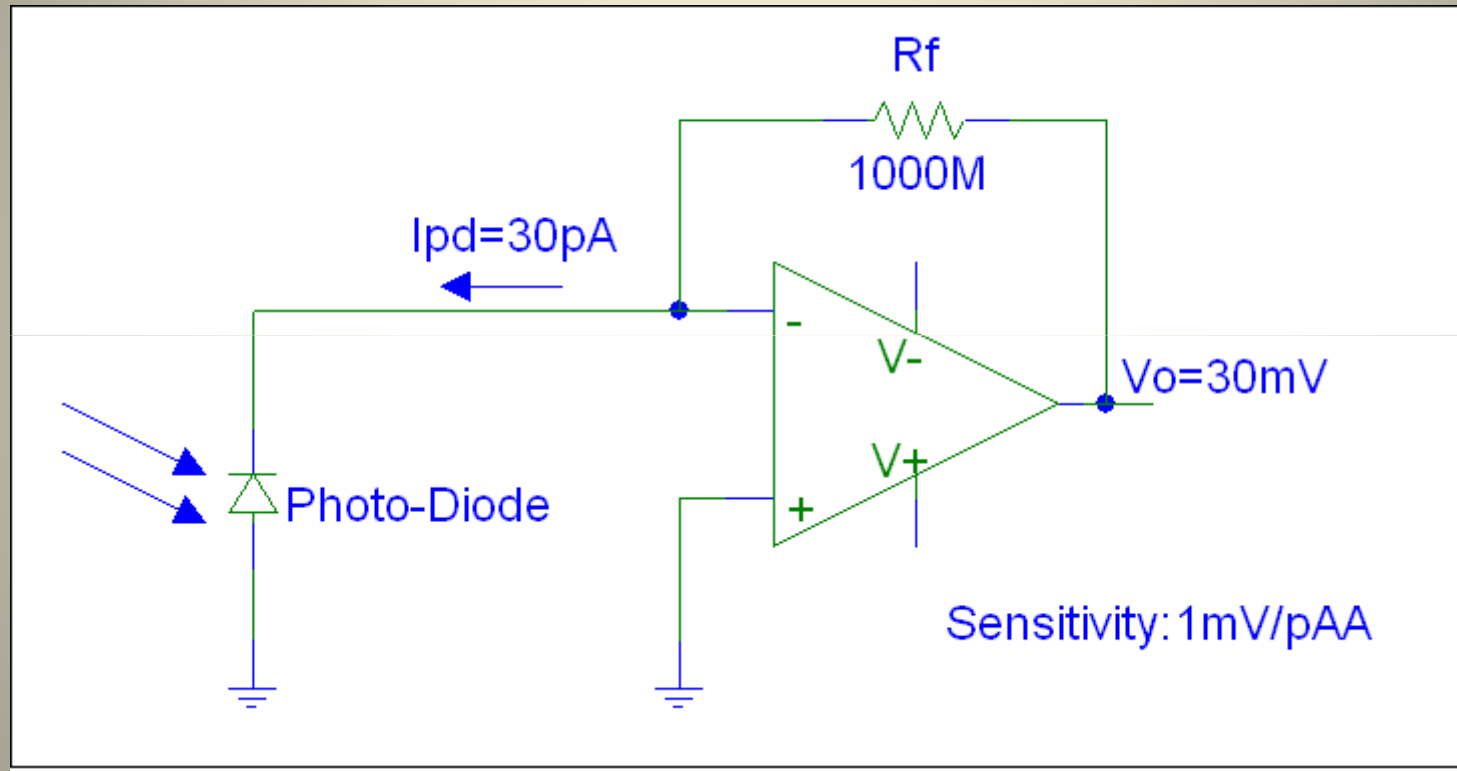
- Primarily light is detected by photodiodes, APDs, photoconductors.
- Current output with high impedance or variable high impedance is mainly obtained.
- Current to voltage circuits are basically used.
- Light may be externally injected into optoelectronic measurement systems by means of Lamps, LEDs and LASERs biased by a current source or voltage to current conversion circuit.

# Equivalent of photodiodes and APDs

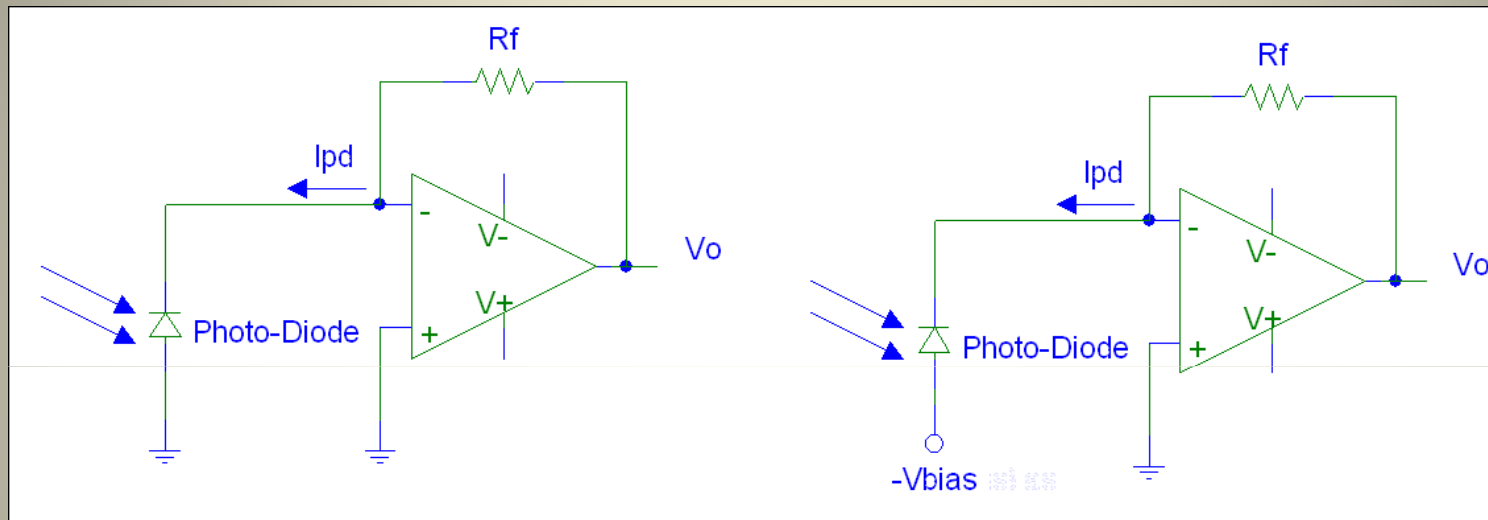




# Current to voltage circuit



# Biassing light detectors



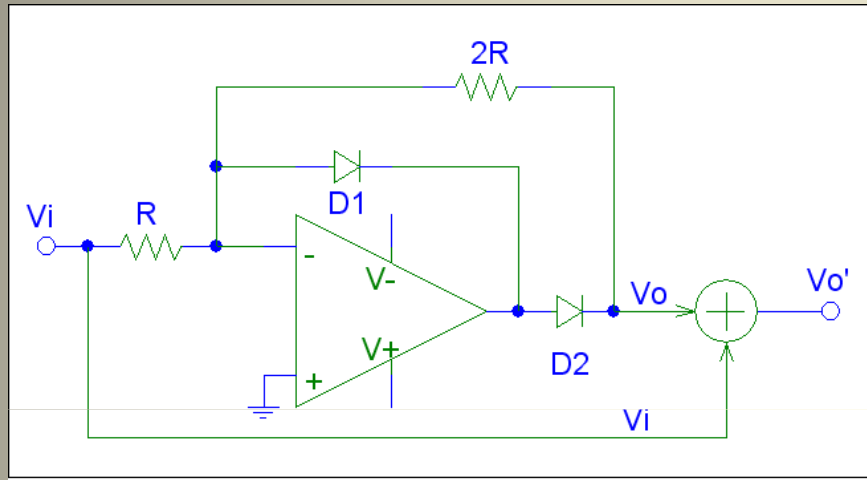
PHOTOVOLTAIC	PHOTOCONDUCTIVE
Zero Bias	Reverse Bias
No "Dark" Current	Has "Dark" Current
Low Noise (Johnson)	Higher Noise (Johnson + Shot)
Precision Applications	High Speed Applications



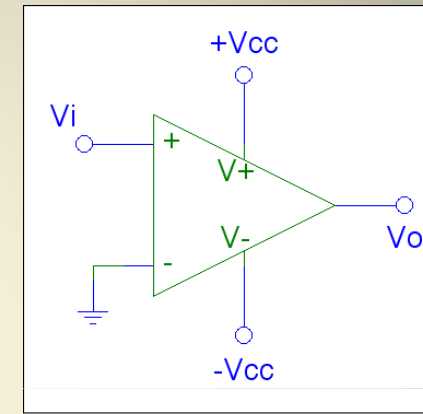
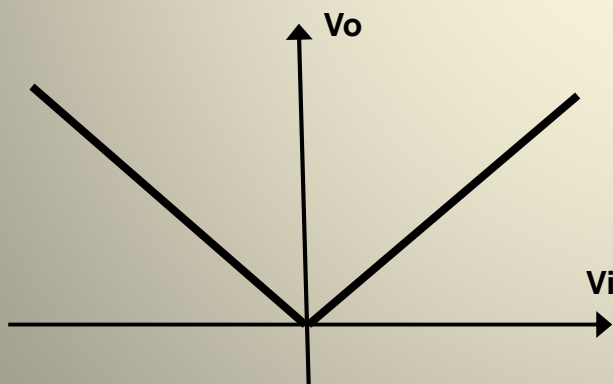
# Non-linear analog signal processing

- Operational Amplifiers are used in saturated mode
- Special Amplifiers and Comparators
- Survey of applications
  - Precision rectifiers, Peak detectors, envelope and RMS detectors
  - Schmitz –trigger comparators
  - Logarithmic amplifier

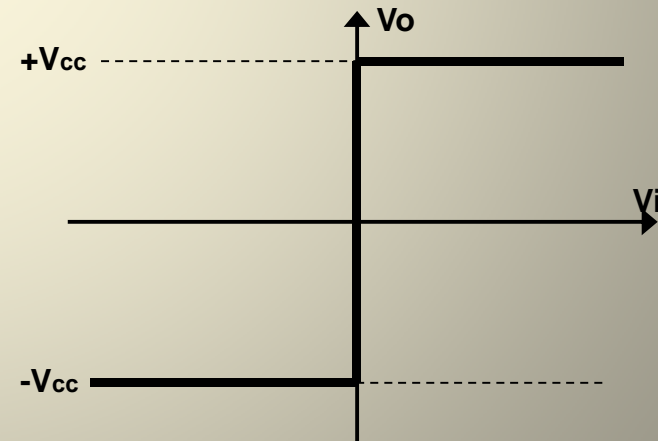
# Examples of Non-linear signal processing



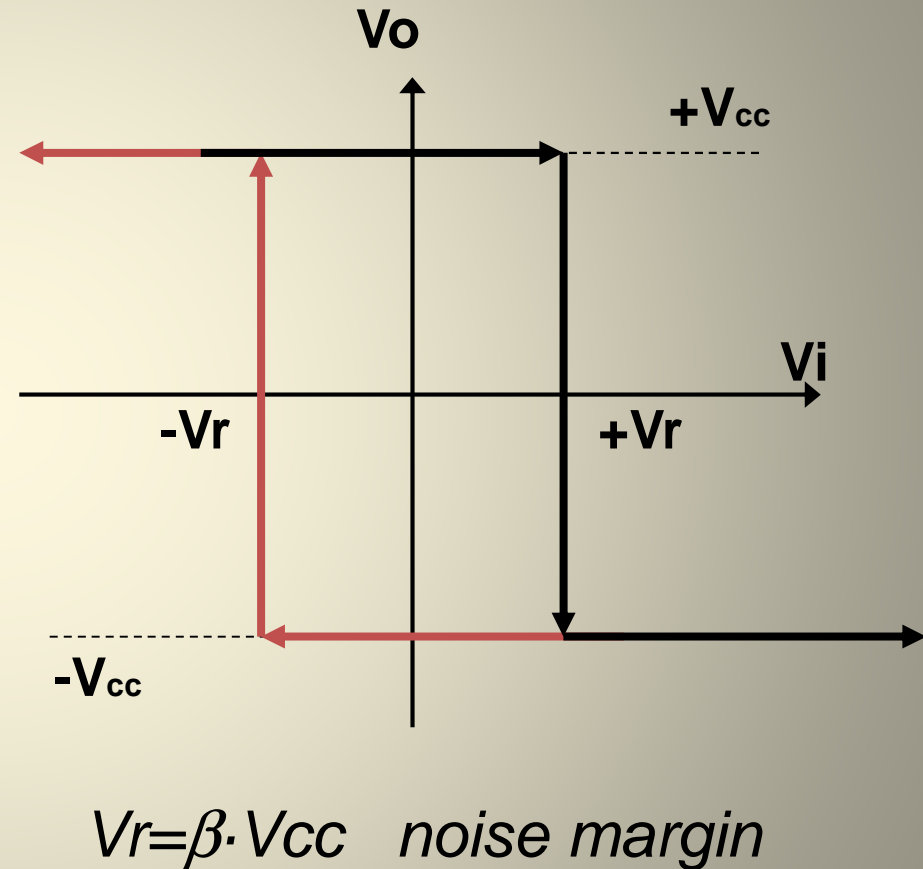
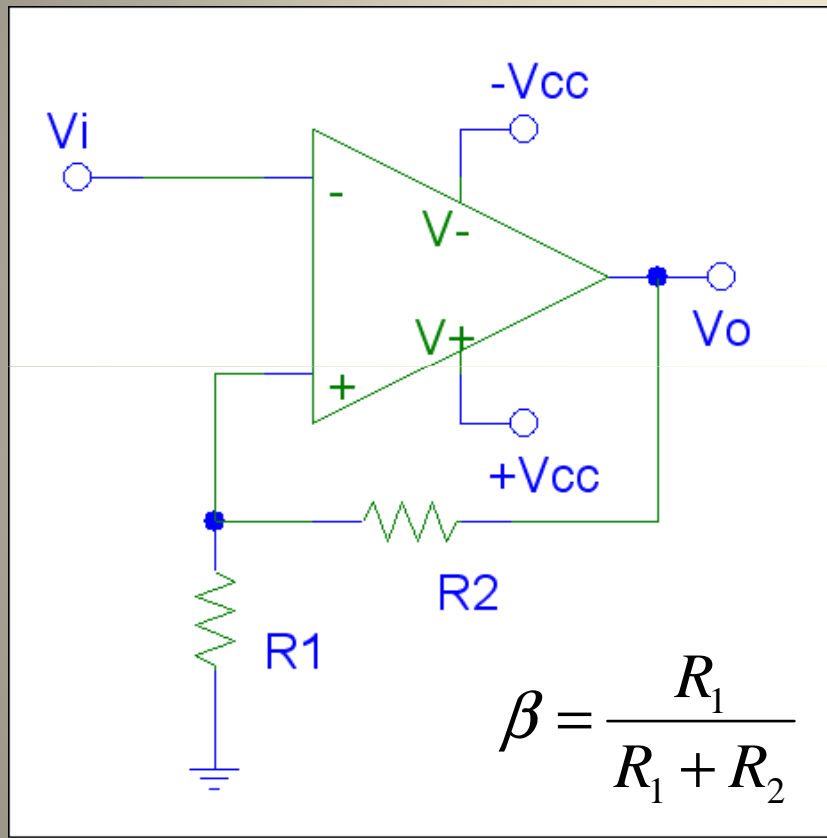
Full-wave precision amplifier



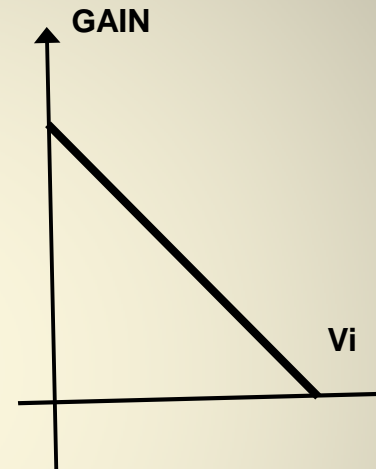
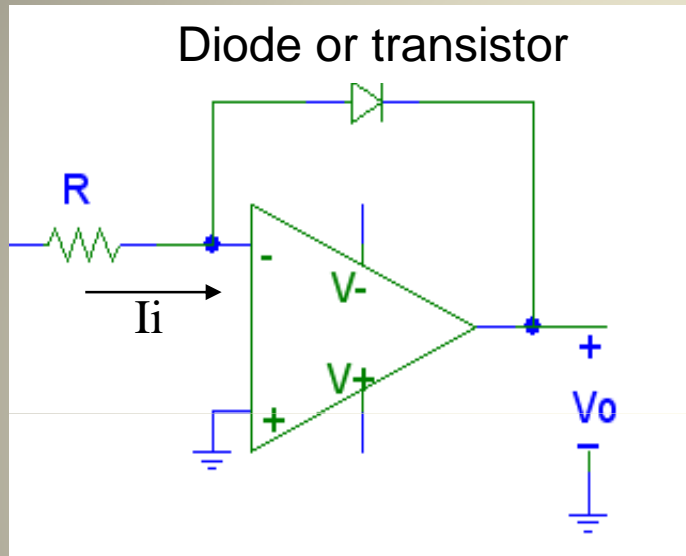
Comparator with zero



# Smith-trigger comparator



# Logarithmic amplifiers



$$V_o = -\frac{KT}{q} \ln[I_i / I_o]$$

Linearization of exponential sensitivity  
Gain change extends the input range

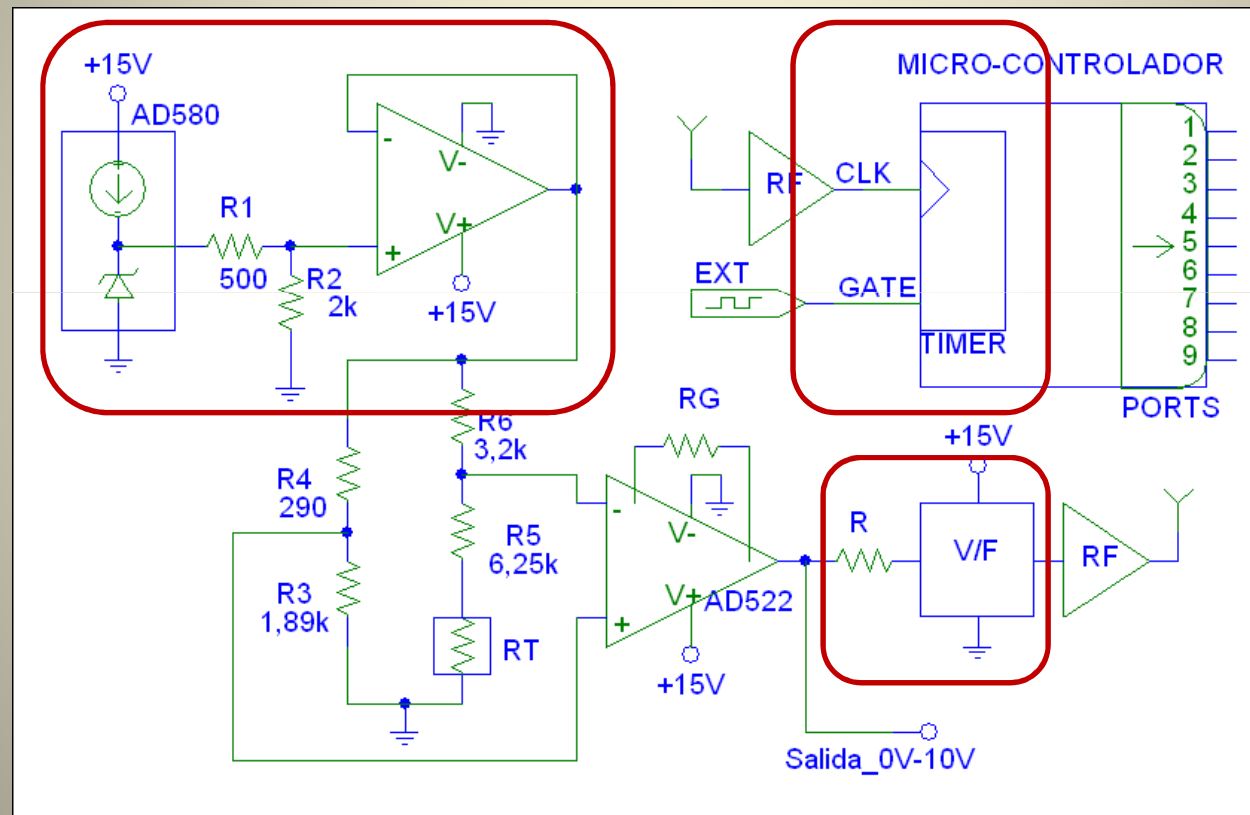
\* Log101



## Special Function Modules

- Multipliers and modulators / demodulators
- Voltage to Frequency converters and frequency detectors

# Example of analog signal conditioning and special function modules



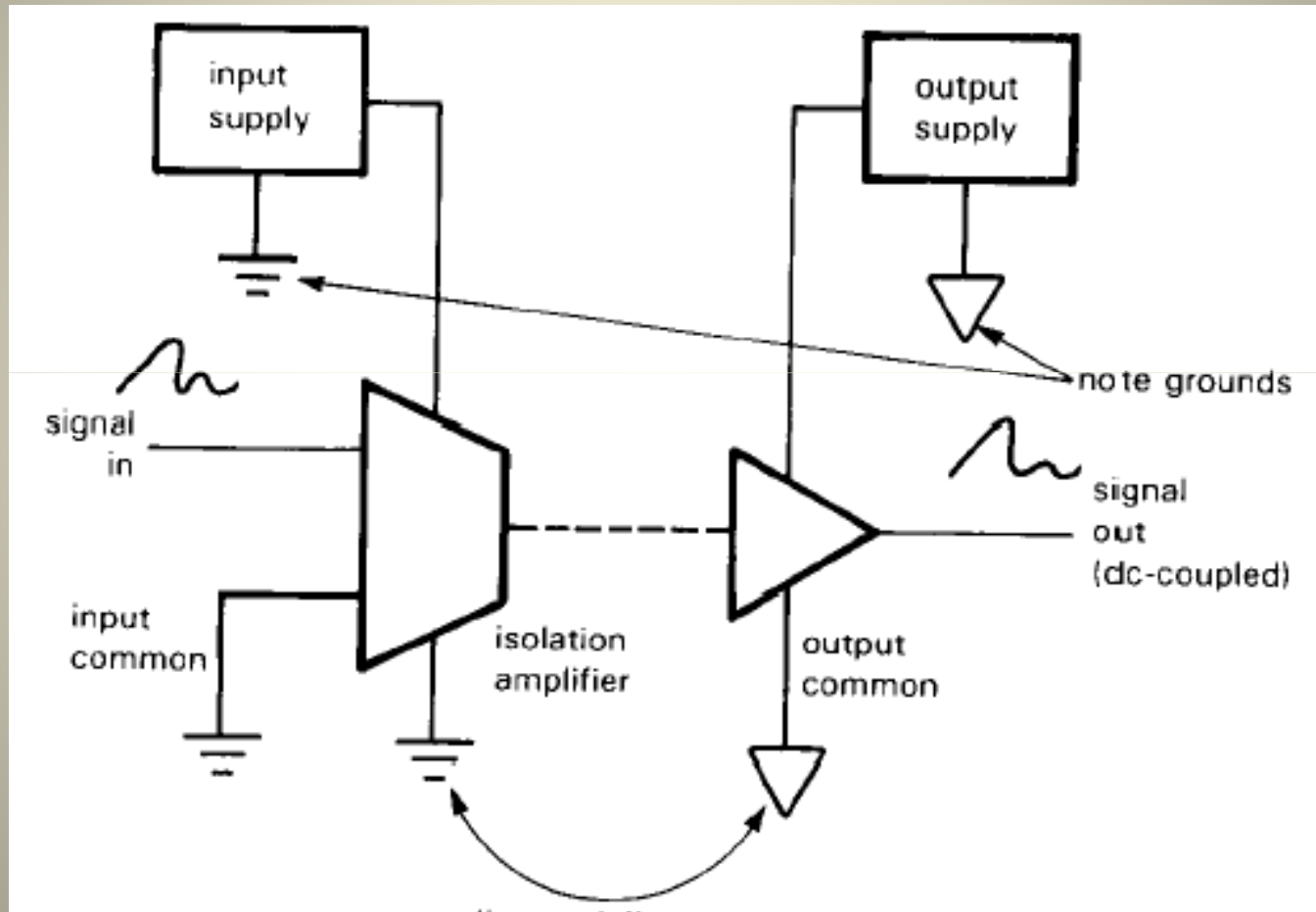




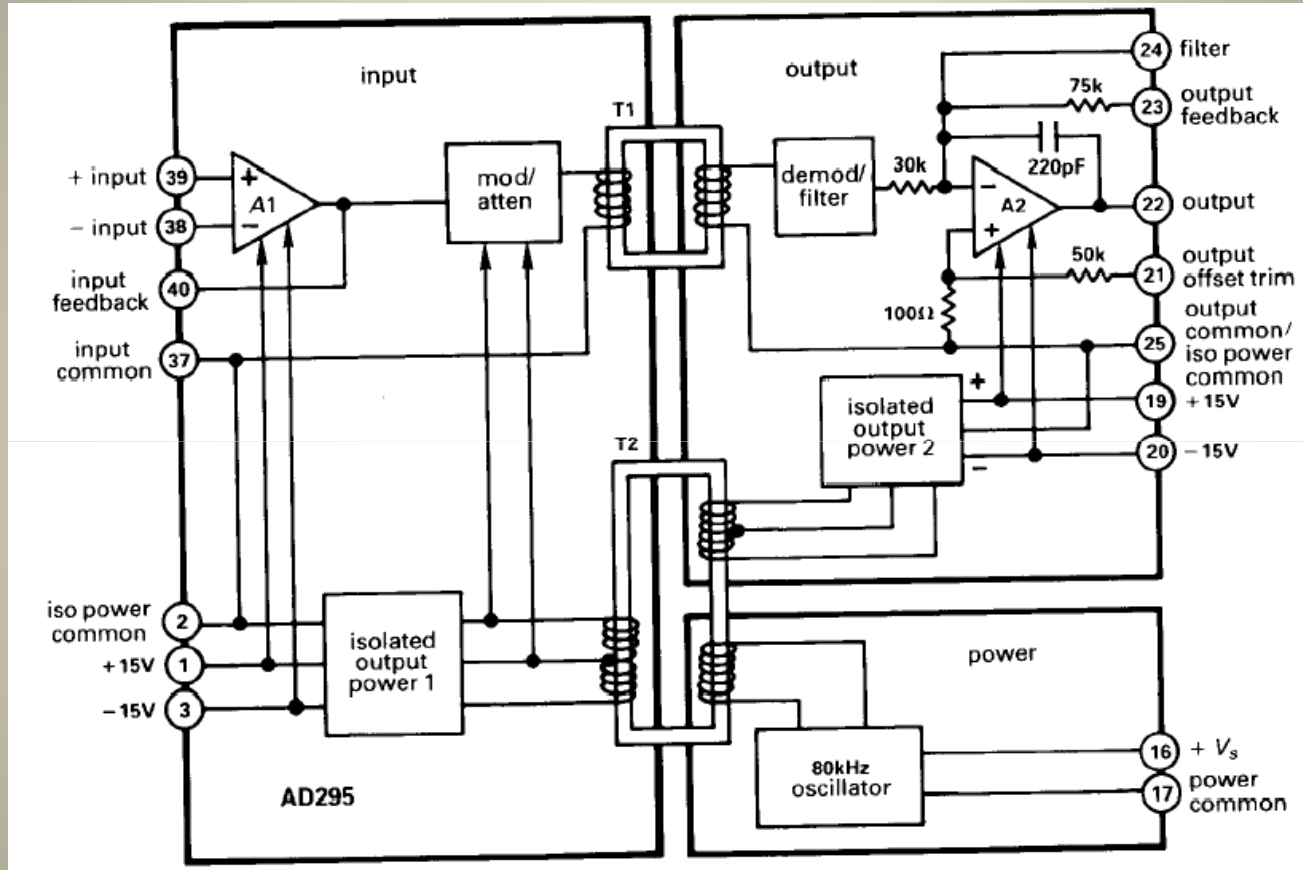
## Other specific instrumentation components and circuits

- Isolation amplifiers
- Auto-zero Amplifiers
- Charge Amplifiers
- Switched-capacitor amplifiers and filters

# Isolation amplifiers basic principles

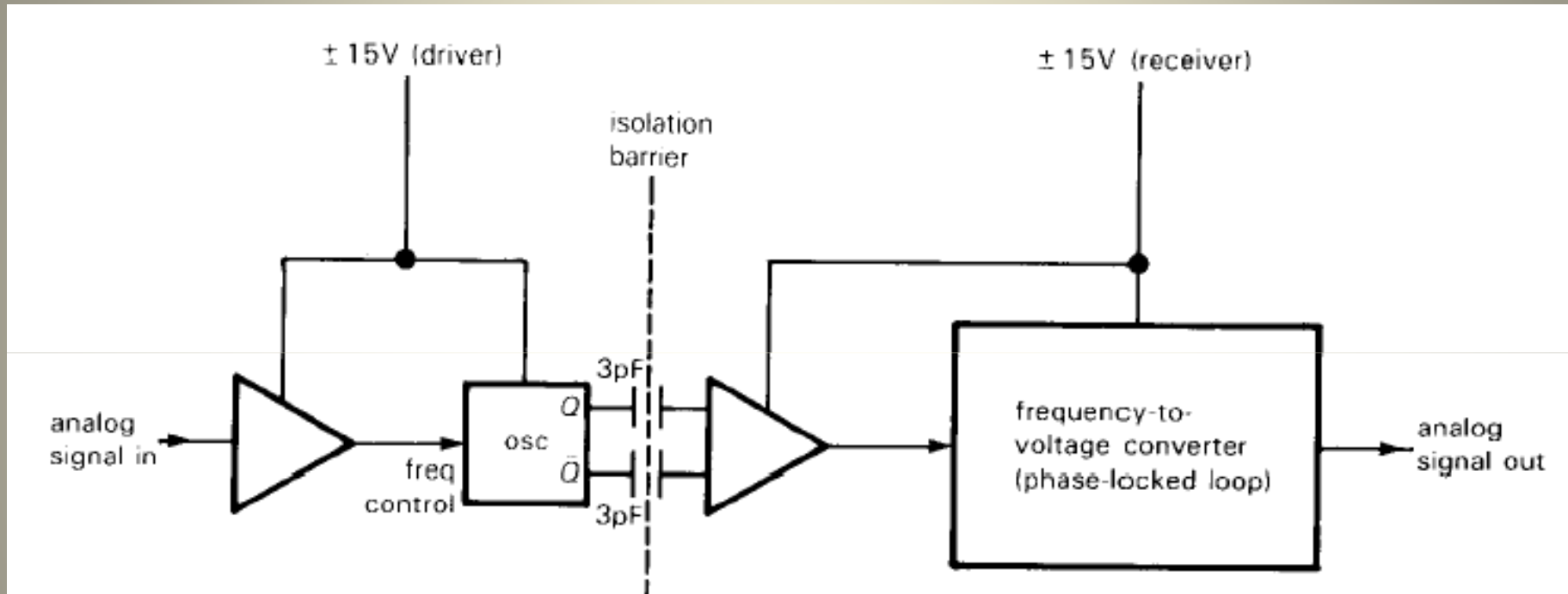


## Transformer (inductive) isolation barrier



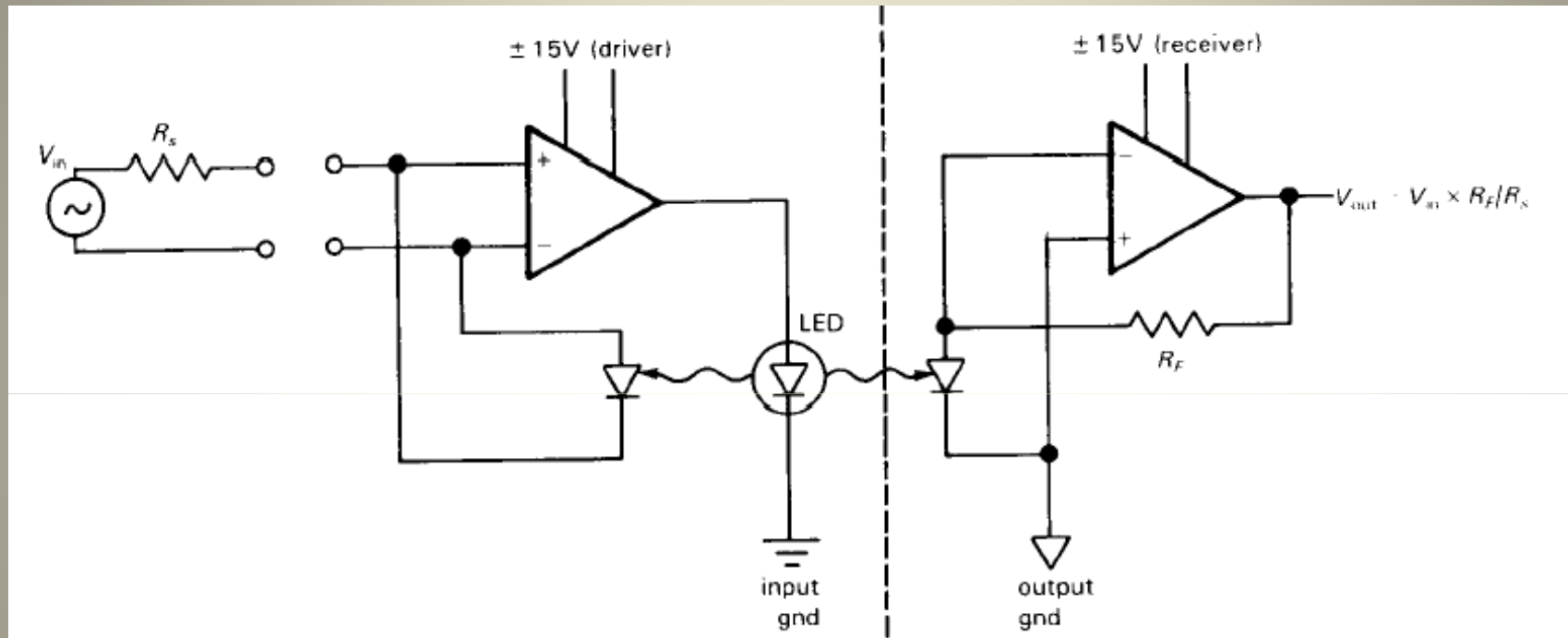
\* AD210

## Capacitive isolation barrier



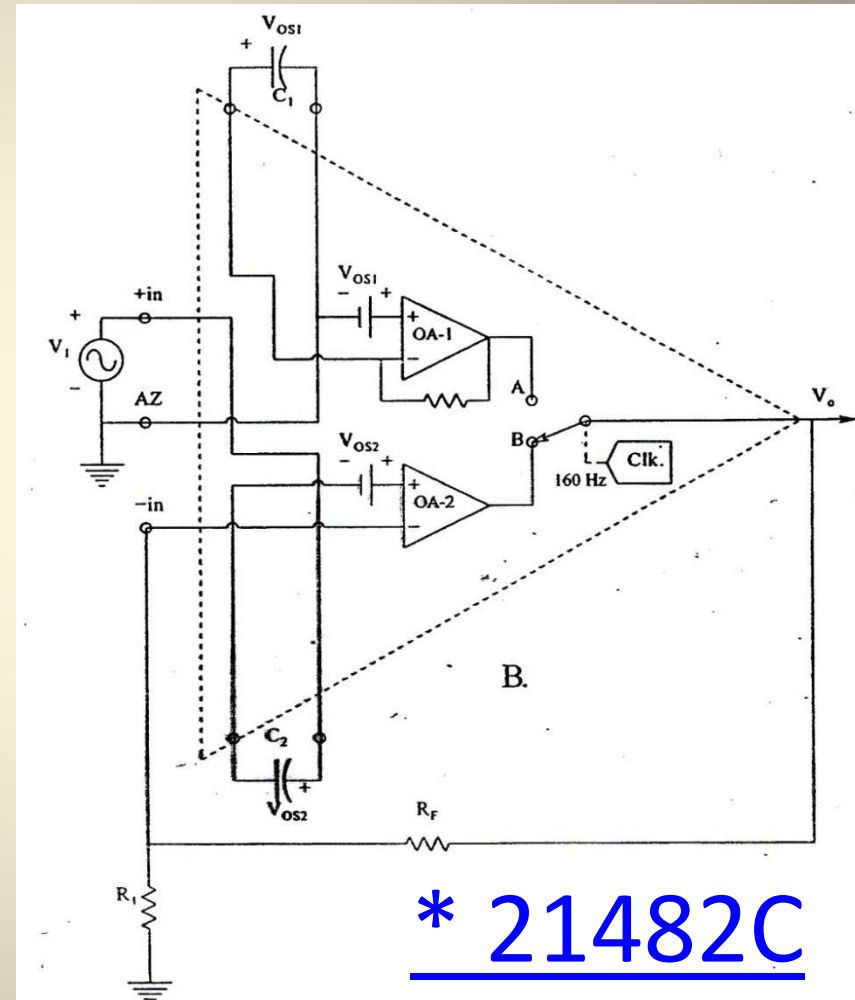
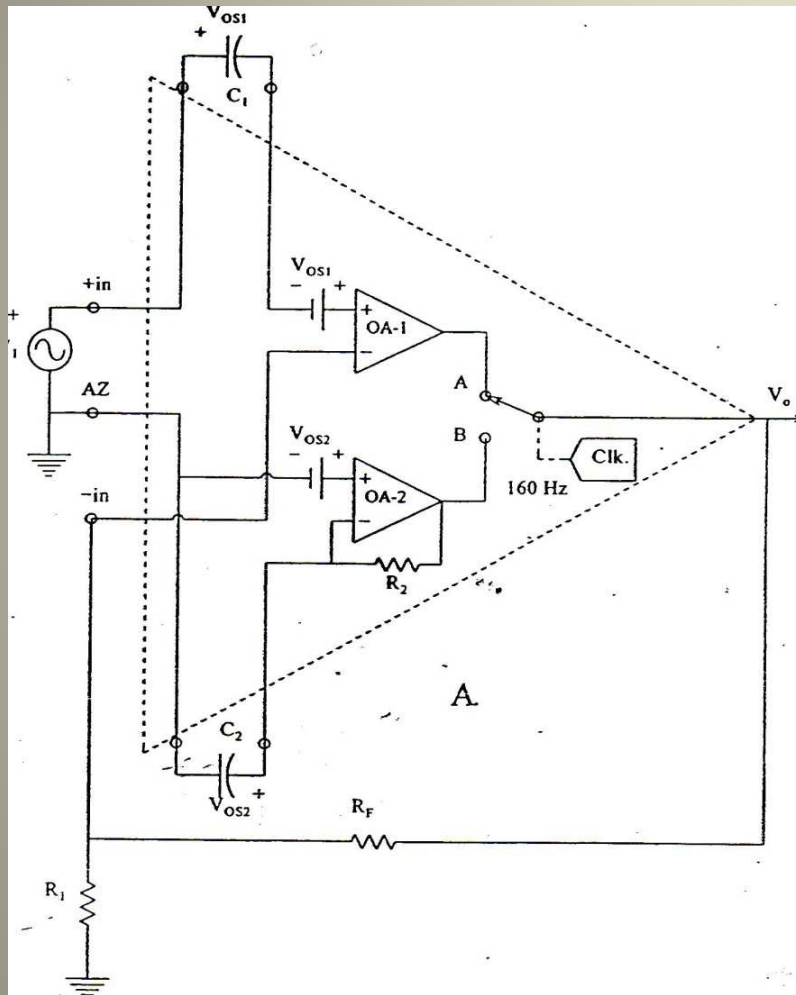
\* Iso102

## Optic isolation barrier

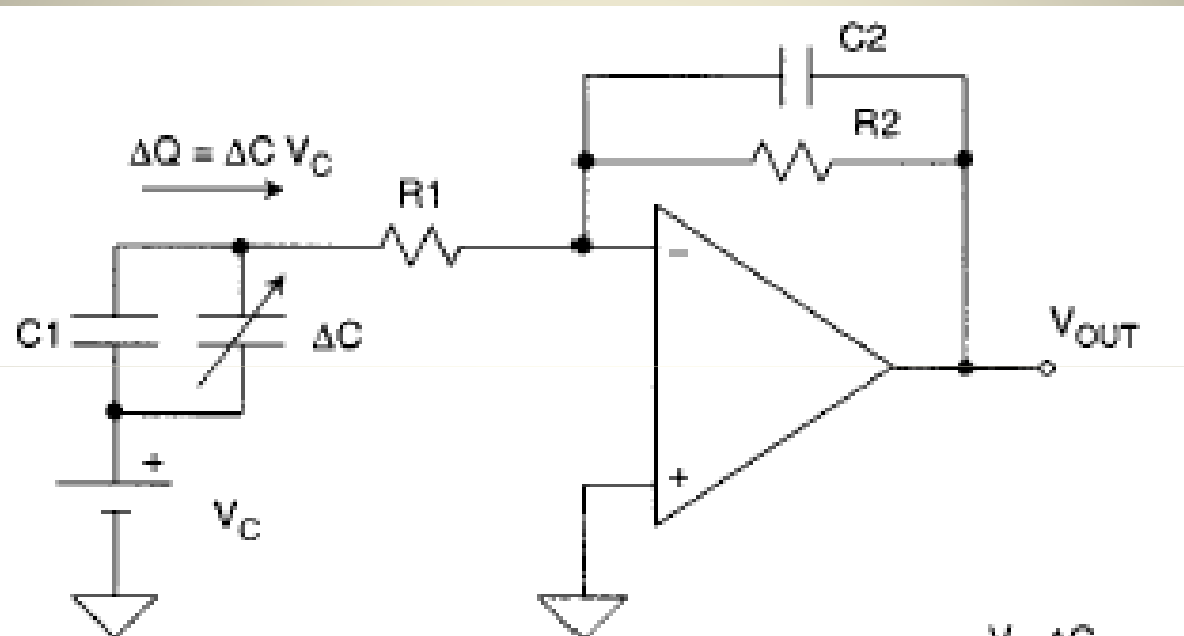


\* Iso100

# Auto-zero Amplifiers

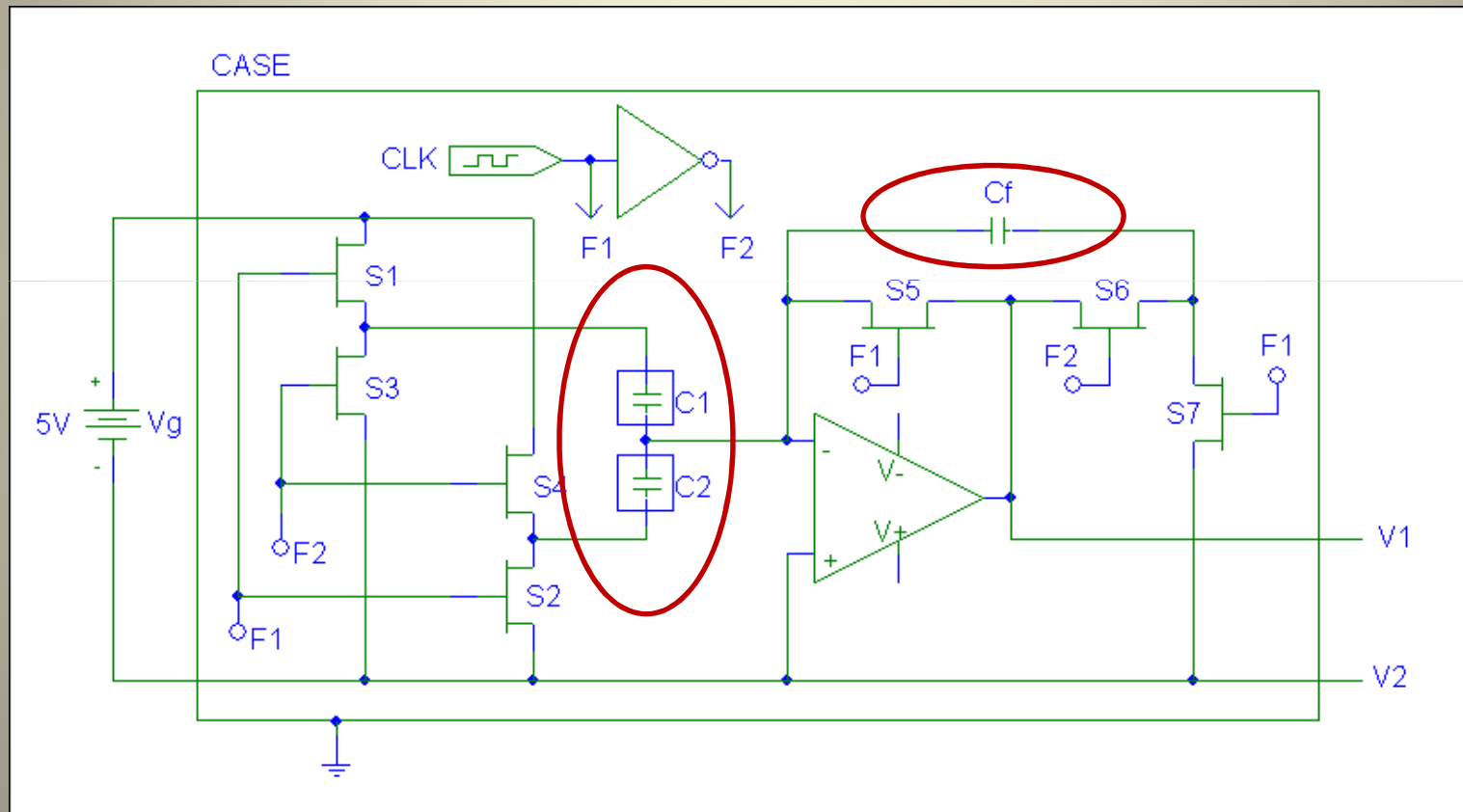


## Charge amplifiers basics



- FOR CAPACITIVE SENSORS:  $\Delta V_{OUT} = \frac{-V_C \Delta C}{C_2}$
- FOR CHARGE-EMITTING SENSORS:  $\Delta V_{OUT} = \frac{-\Delta Q}{C_2}$

# Switched-capacitor amplifier basics







# Summary

- We have described the basis for passive sensors signal conditioning, stressing the importance of the influence variables and null conditioning schemes.
- Instrumentation amplifiers have also been presented as main components in instrumentation systems where differential signals are present.
- Several schemes for analog signal condition, linear and nonlinear, based on operational amplifiers have also been presented.
- Finally, other specific instrumentation components and circuits have also been presented.