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Session 19

Frequency Response of Transistor Amplifiers

Electronic Components and Circuits

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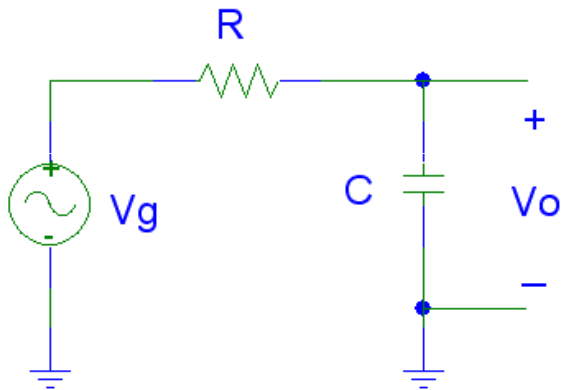
Frequency Response of Transistor Amplifiers

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Fundamentals

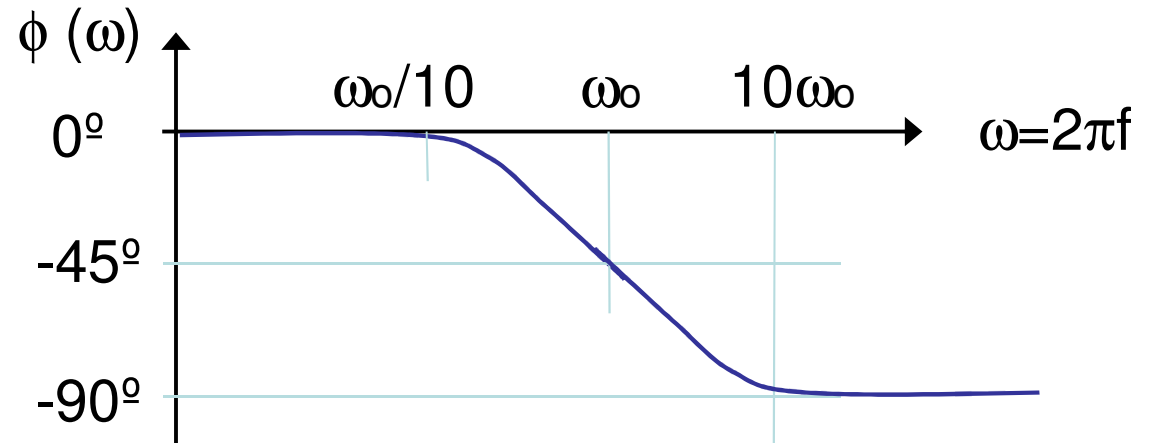
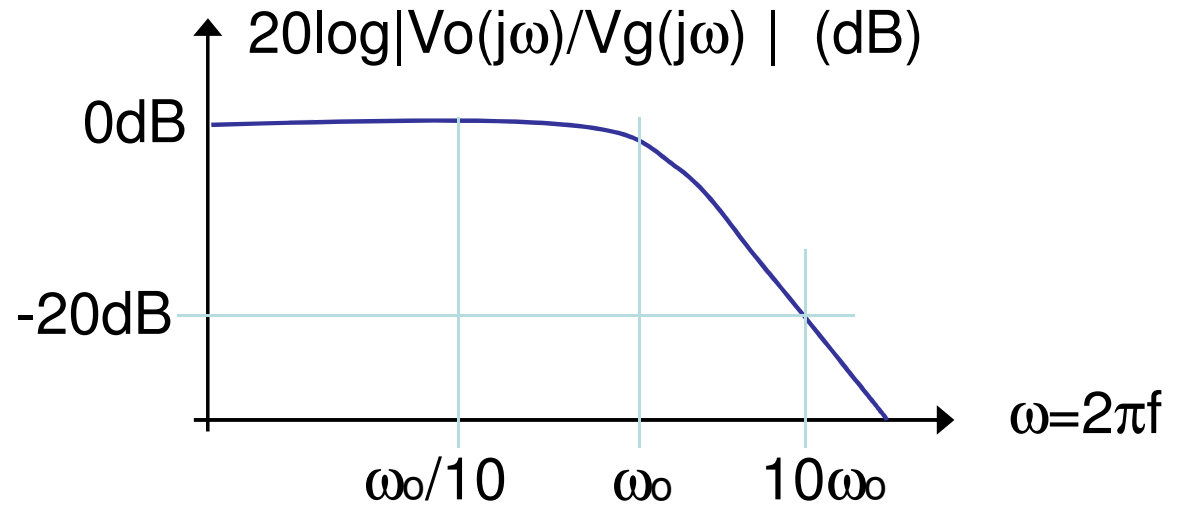
Low-pass RC Circuit



$$T(s) = \frac{V_o}{V_g} = \frac{1}{1 + (s/\omega_0)}$$

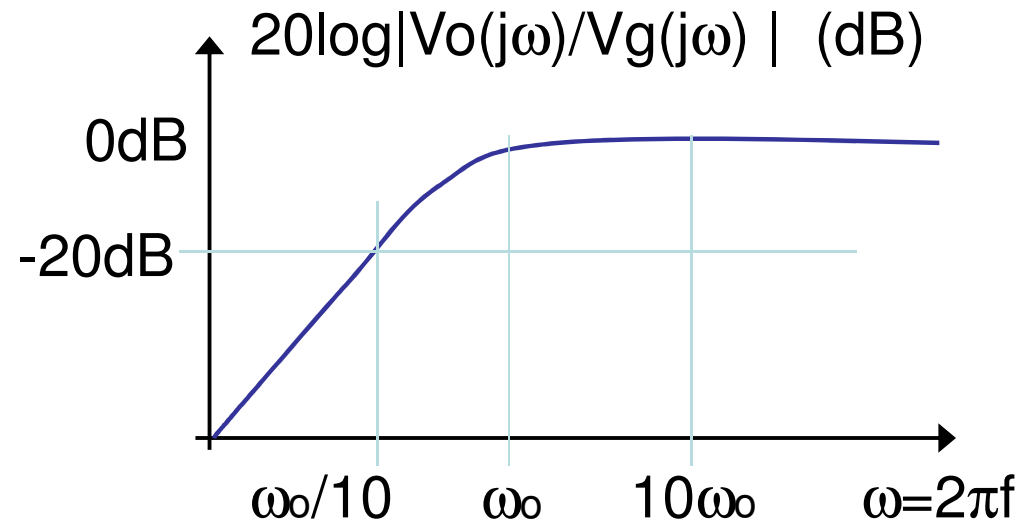
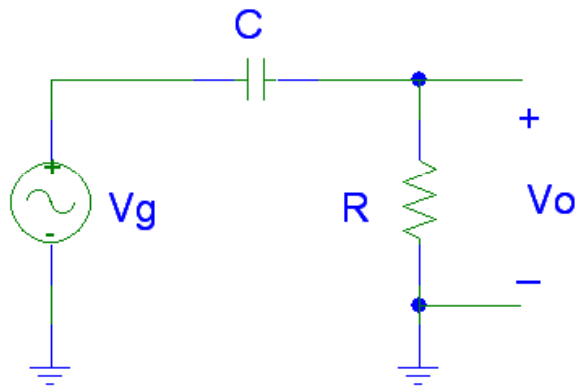
$$|T(j\omega)| = \frac{1}{\sqrt{1 + (\omega/\omega_0)^2}}$$

$$\phi(\omega) = -\tan^{-1}(\omega/\omega_0)$$



Fundamentals

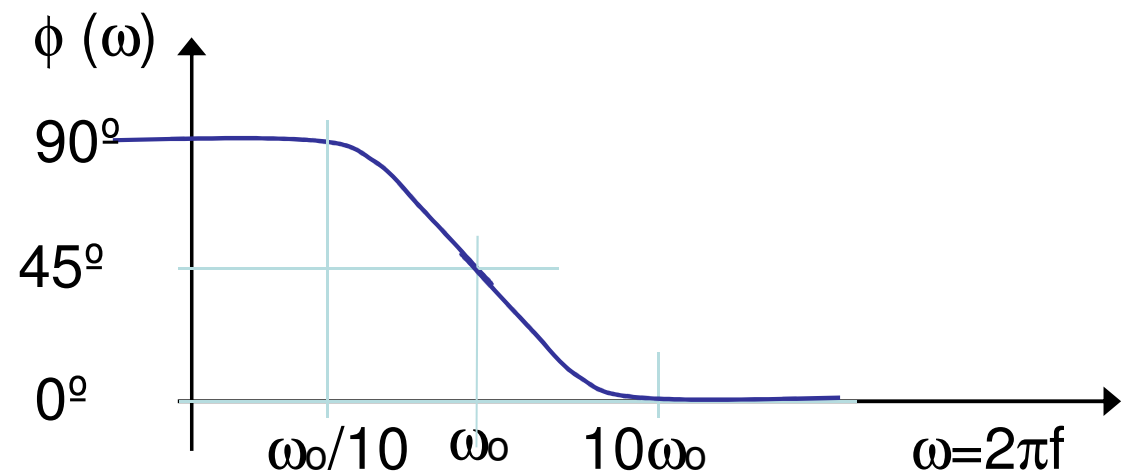
High-pass RC Circuit



$$T(s) = \frac{V_o}{V_g} = \frac{s}{s + \omega_0}$$

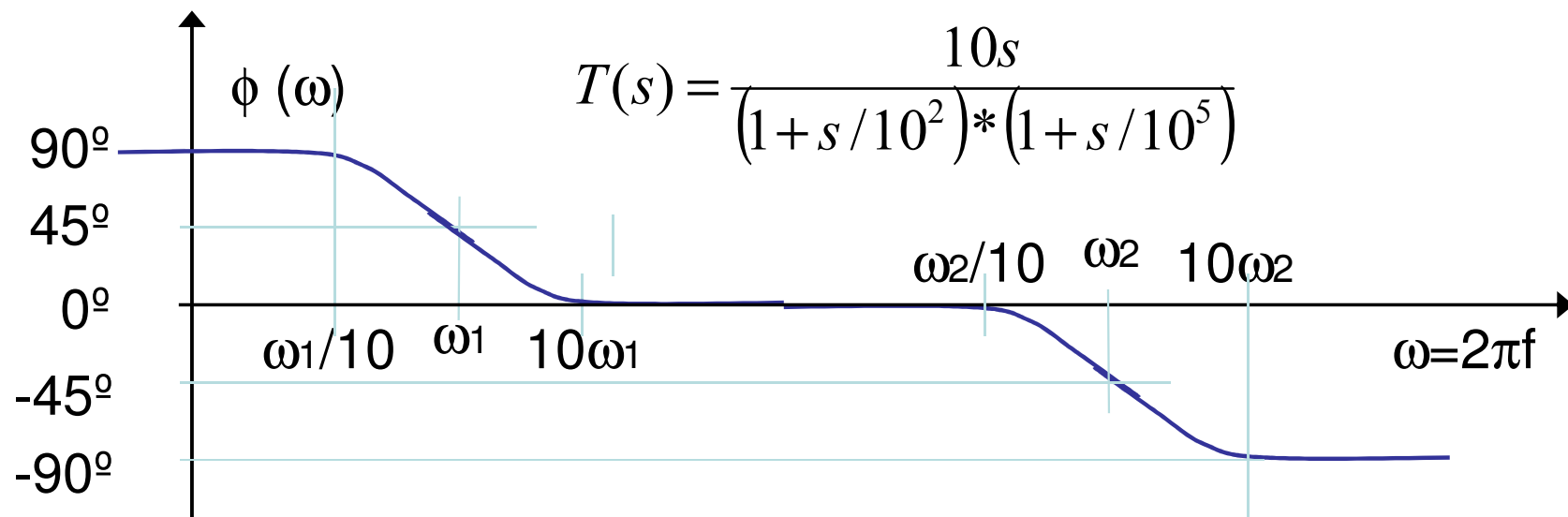
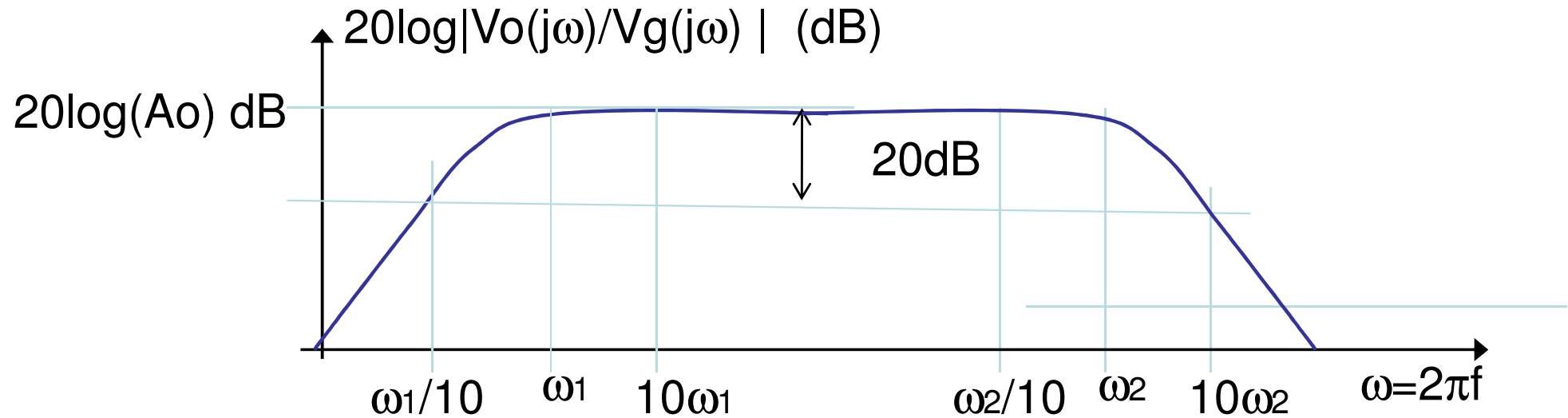
$$|T(j\omega)| = \frac{1}{\sqrt{1 + (\omega_0 / \omega)^2}}$$

$$\phi(\omega) = \tan^{-1}(\omega_0 / \omega)$$

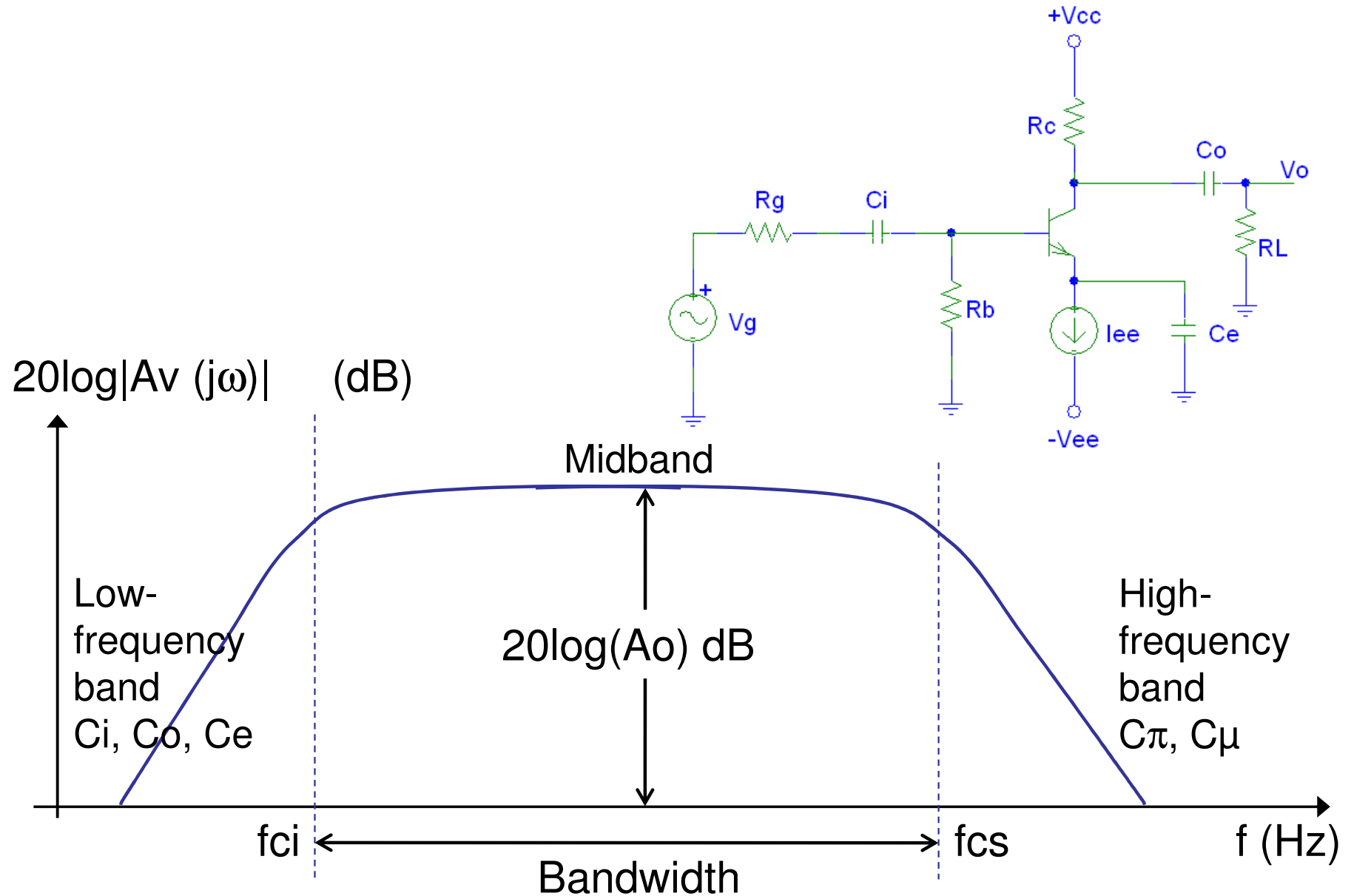


Fundamentals

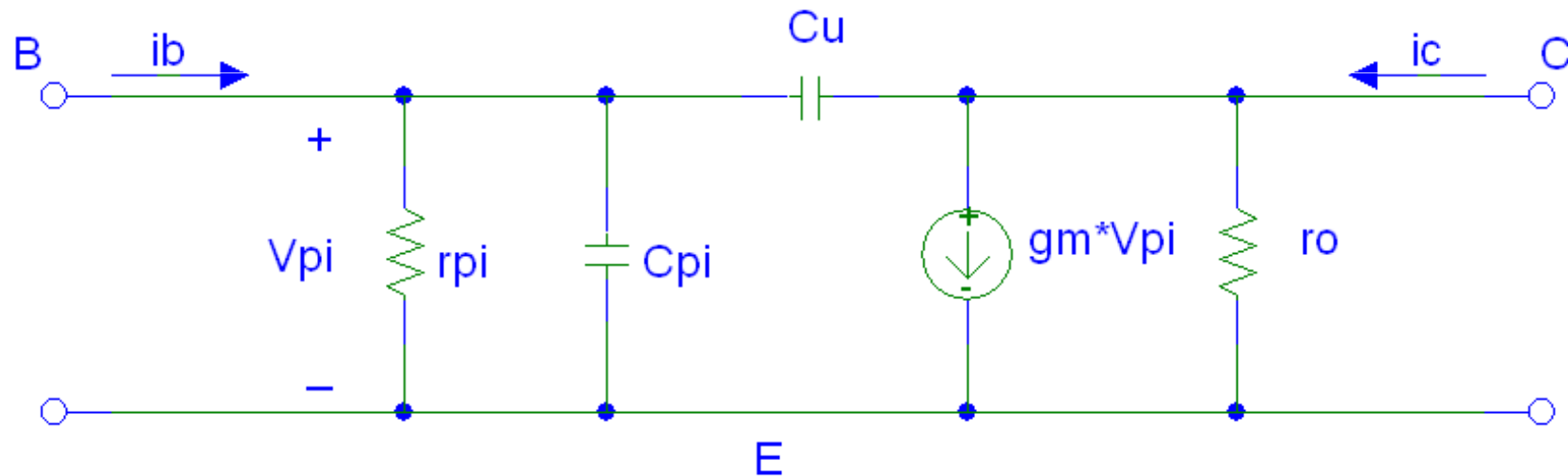
Bode Plot (Amplitude and Phase)



Fundamentals: The three Frequency Bands



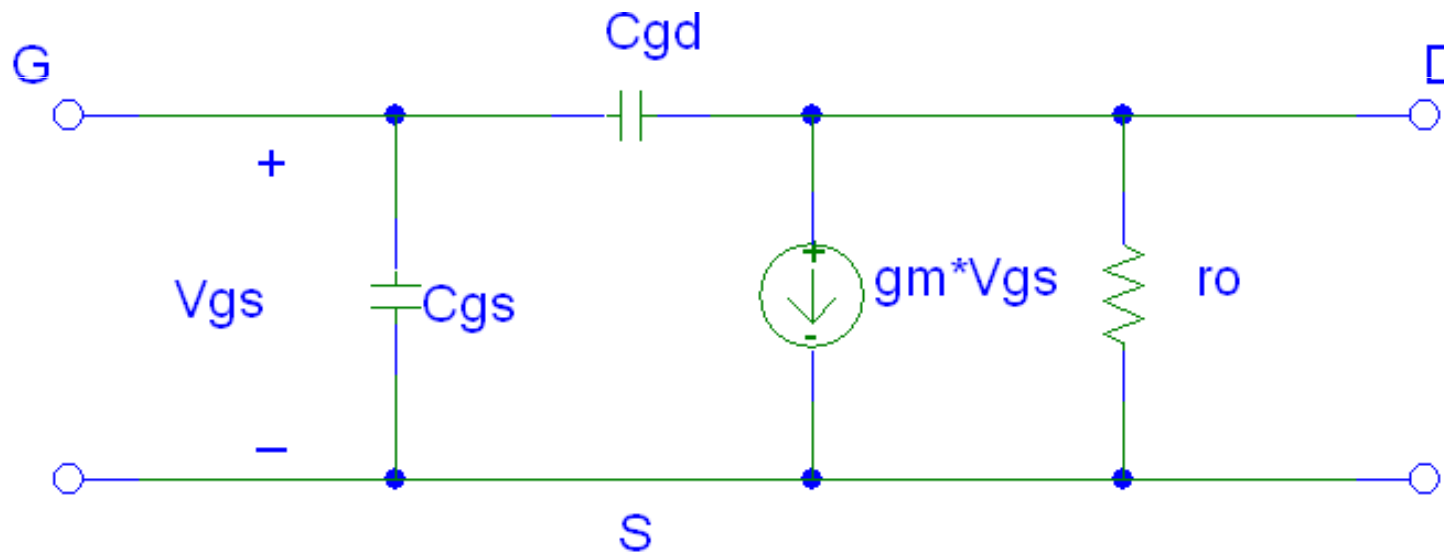
BJT high-frequency small-signal model



Unity-gain
bandwidth

$$f_T = \frac{g_m}{2\pi(C_\pi + C_\mu)}$$

FET high-frequency small-signal model



Unity-gain
bandwidth

$$f_T = \frac{g_m}{2\pi(C_{gs} + C_{gd})}$$

High-frequency response analysis of amplifier circuits.

- High frequency response of transistor amplifier circuits is fixed by the internal capacitances of the devices and the associated time constants.
- In general, we will assume that the high-frequency response is fixed by a DOMINANT POLE. This way, the high-frequency analysis is reduced to the calculation of such dominant pole.
- The dominant pole frequency calculation will be performed using the Open-circuit time constants method.

Open-circuit time constants method.

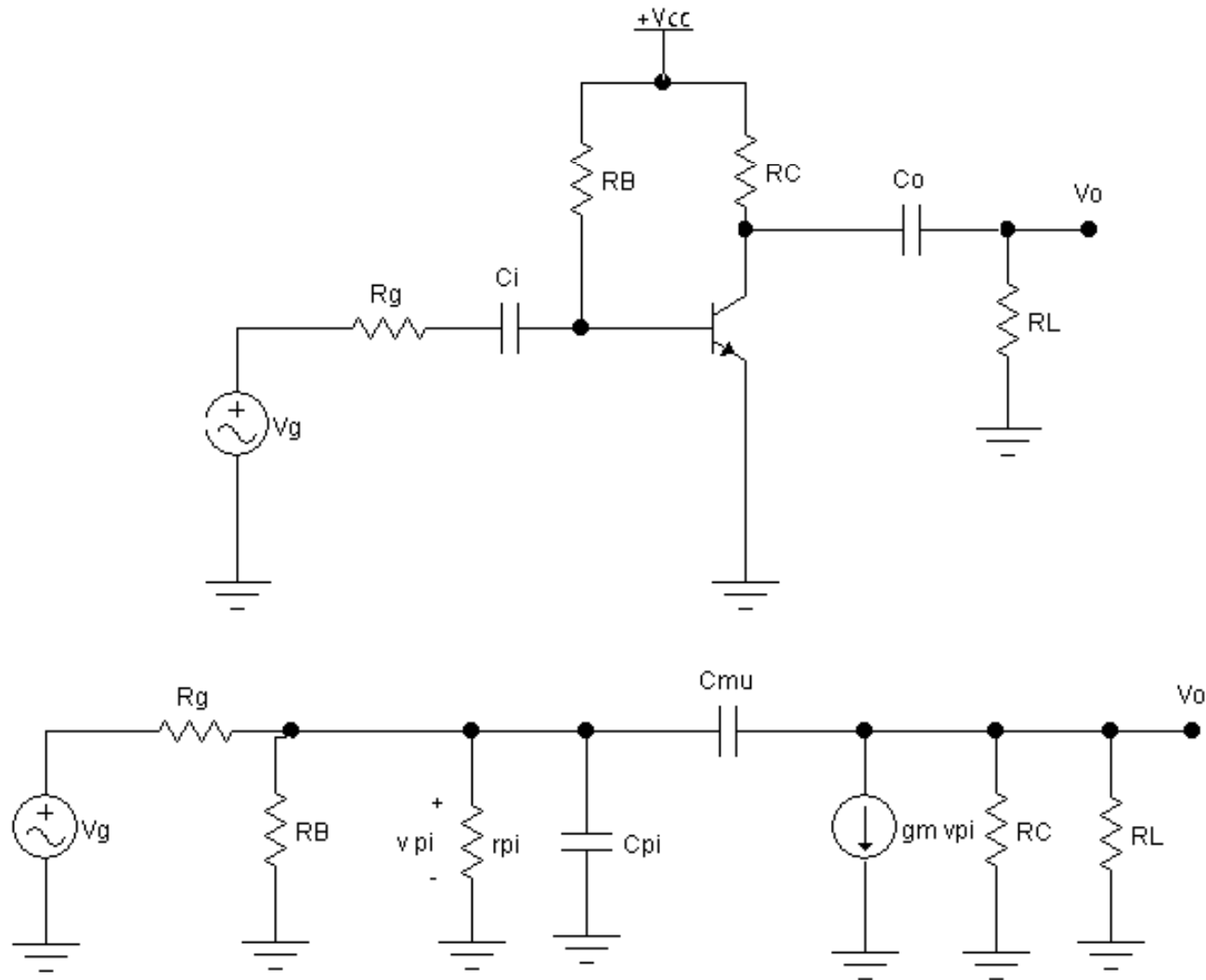
$$f_{cs} (3dB) = \frac{1}{2\pi} \frac{1}{\sum_i R_i^0 C_i}$$

Where:

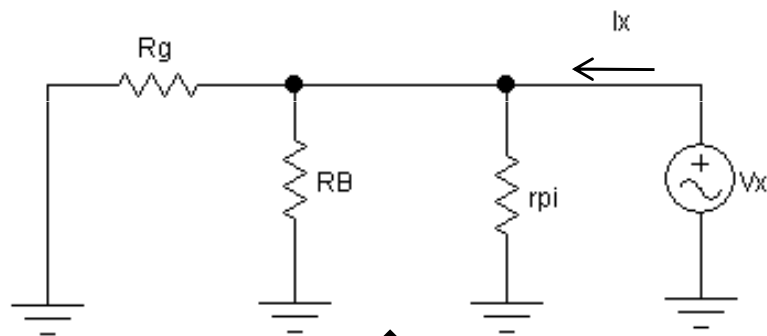
C_i are all the capacitances that influence in the high-frequency response: active devices internal capacitances, or small capacitors (with low-pass characteristics), introduced in the circuit to control the high-frequency response.

R_i^0 is the resistance seen by each of the capacitors when we reduce all other capacitances to zero (Open circuit)

Open-circuit time constants method. Example (I)

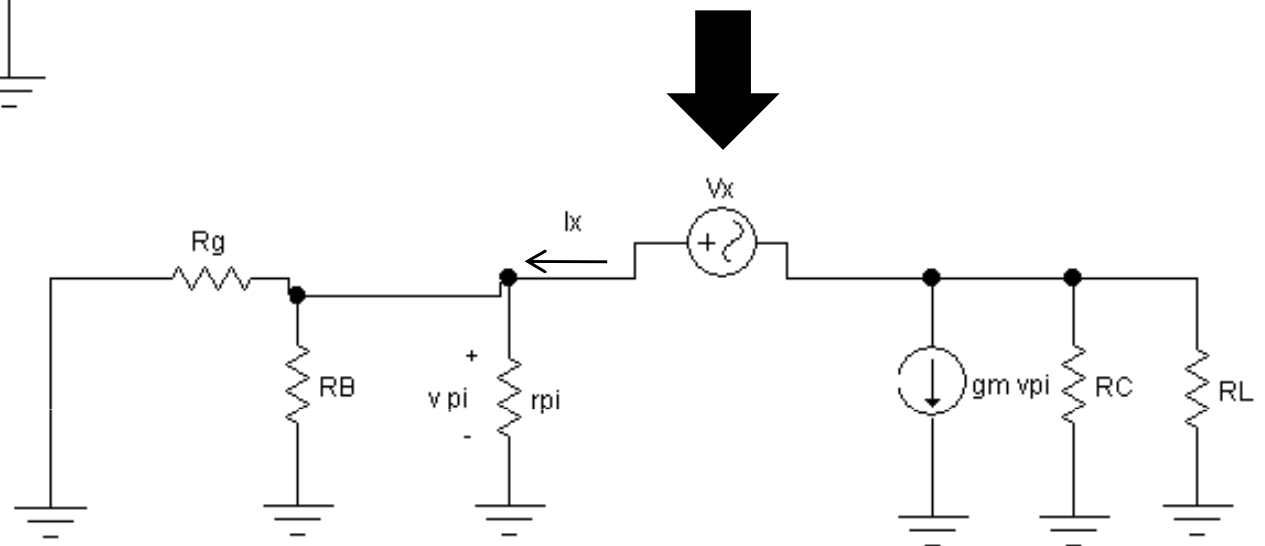


Open-circuit time constants method. Example (II)



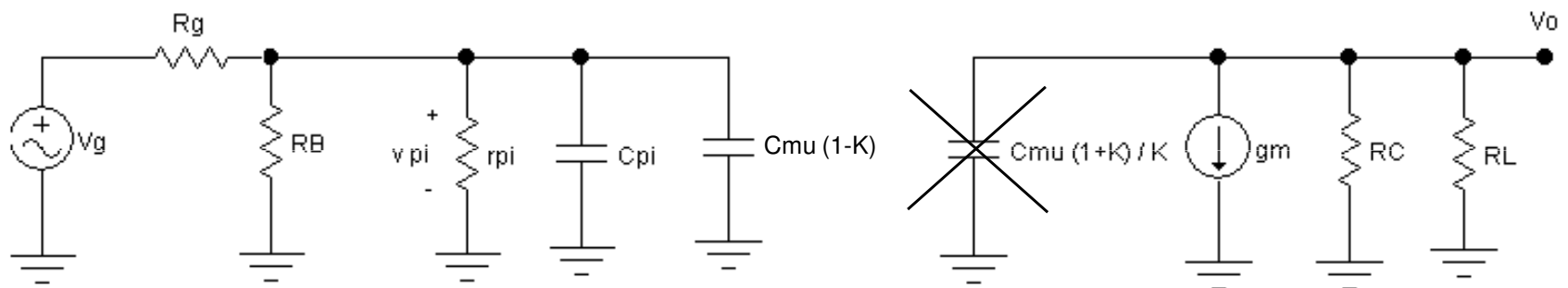
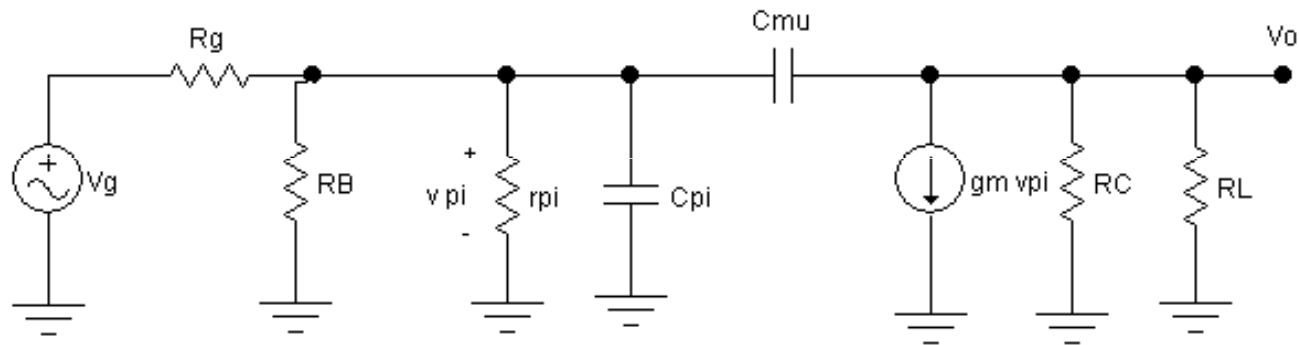
$$R_{\pi}^0 = R_B // r_{\pi} // R_g$$

$$R_{\mu}^0 = R_B // r_{\pi} // R_g (1 + g_m R_C // R_L) + R_C // R_L$$



$$f_{cs} = \frac{1}{2\pi C_{\pi} (r_{\pi} // R_B // R_g) + C_{\mu} (R_B // r_{\pi} // R_g (1 + g_m R_C // R_L) + (R_C // R_L))}$$

Miller's Theorem. Example (I)



$$K = -gm R_C // R_L$$

Miller's Theorem. Example (II)

Miller's Theorem vs Dominant Pole Calculation

$$f_{csM} = \frac{1}{2\pi (r_{\pi} // R_B // R_g)} \frac{1}{[C_{\pi} + C_{\mu}(1 + g_m R_C // R_L)]}$$

$$f_{cs} = \frac{1}{2\pi C_{\pi} (r_{\pi} // R_B // R_g) + C_{\mu} (R_B // r_{\pi} // R_g (1 + g_m R_C // R_L) - R_C // R_L)}$$

Low-frequency response analysis of amplifier circuits.

- Low-frequency response of transistor circuits is fixed by the coupling and bypass capacitors and the associated time constants.
- In general, we will assume that the low-frequency response is fixed by a DOMINANT POLE. This way, the low-frequency analysis is reduced to the calculation of such dominant pole.
- The dominant pole frequency calculation will be performed using the Short-circuit time constants method.

Short-circuit time constants method.

$$f_{ci} (3dB) = \frac{1}{2\pi} \sum_i \frac{1}{R_i^\infty C_i}$$

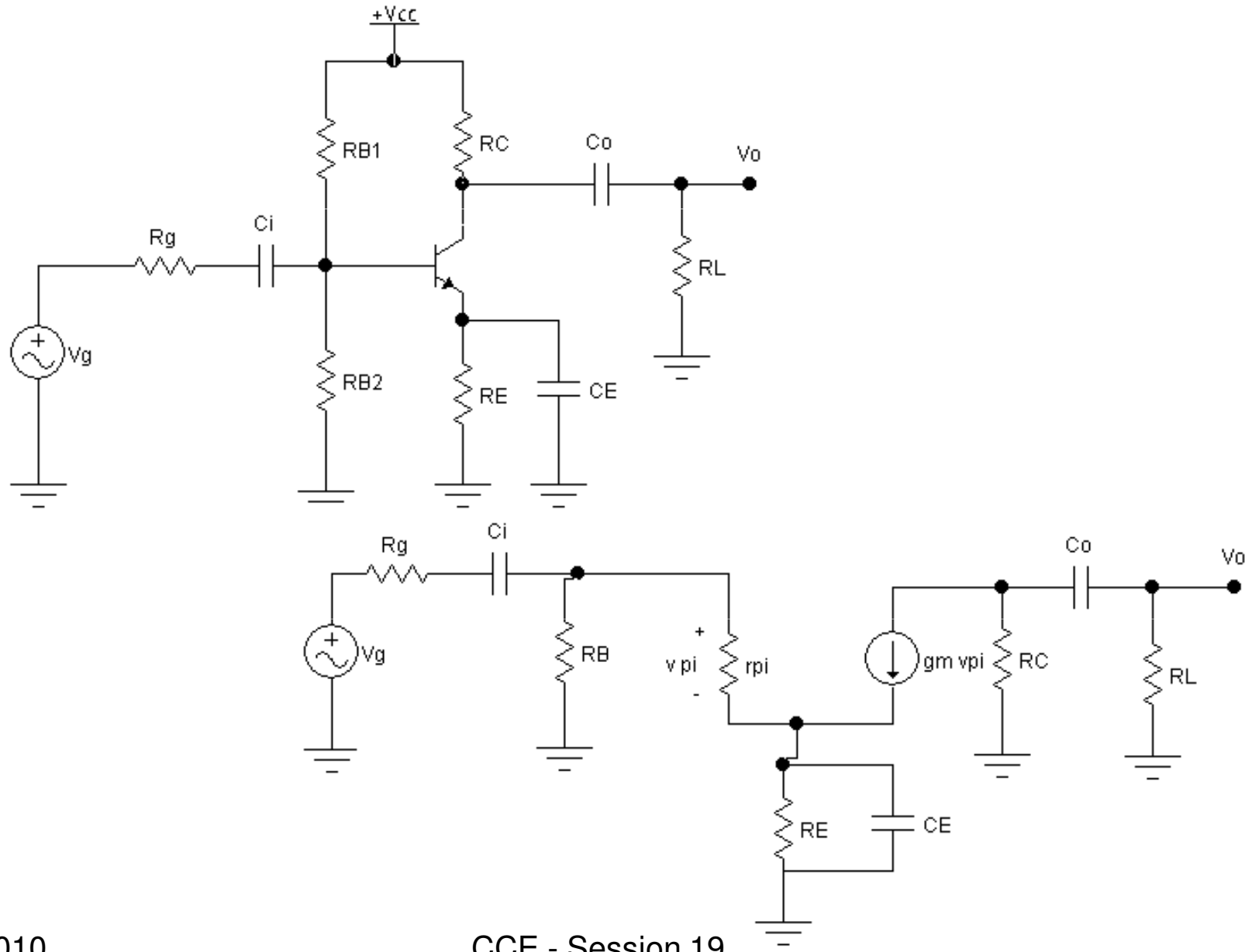
Where:

C_i are all the coupling and bypass capacitors of the circuit.

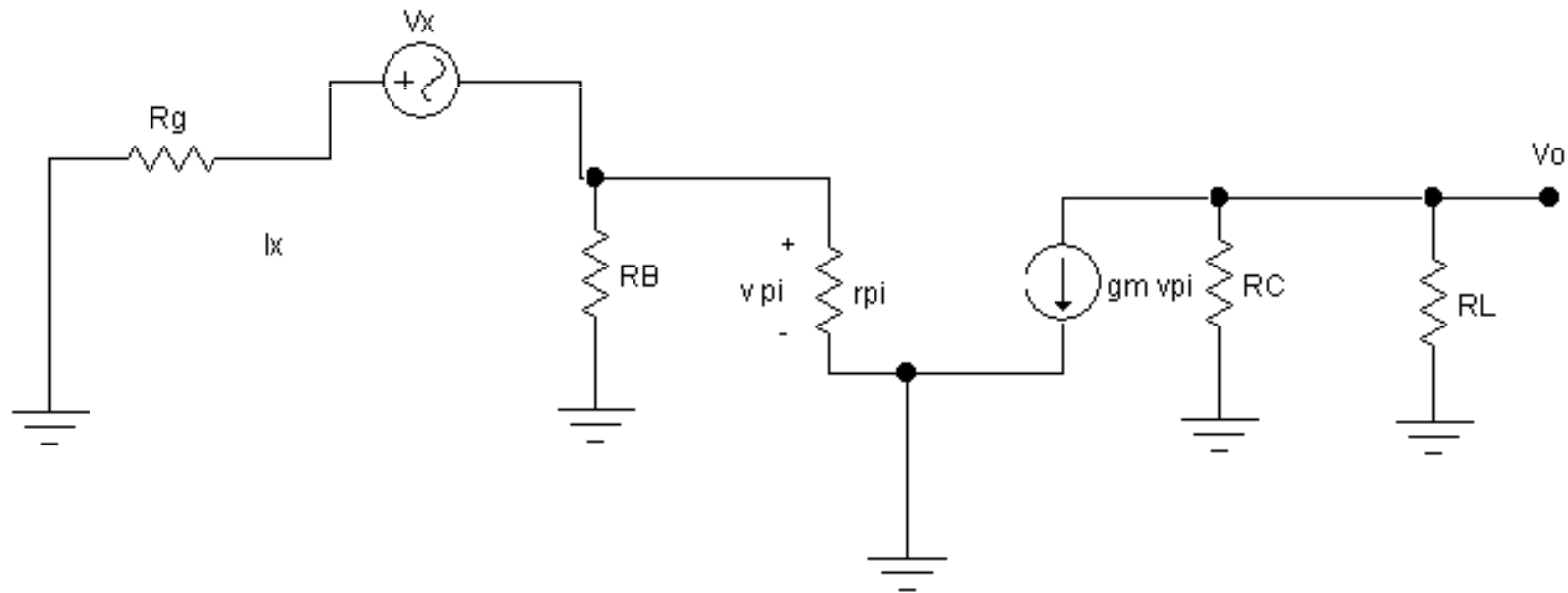
R_i^∞ is the resistance seen by each of the capacitors when we assume all other capacitances are infinity (Short circuit)

Short-circuit time constants method.

EXAMPLE (I)

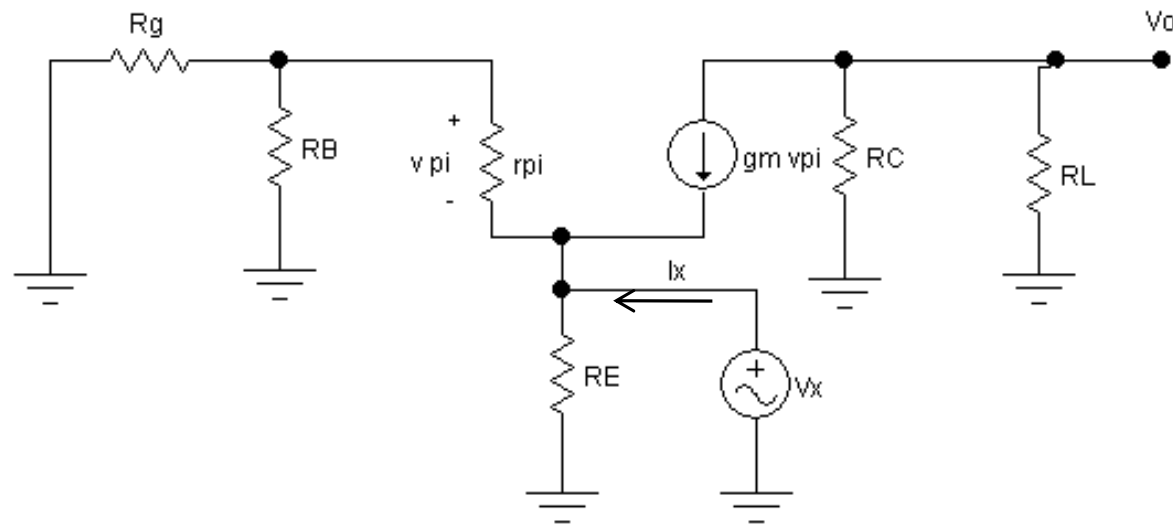


Short-circuit time constants method. EXAMPLE (II)



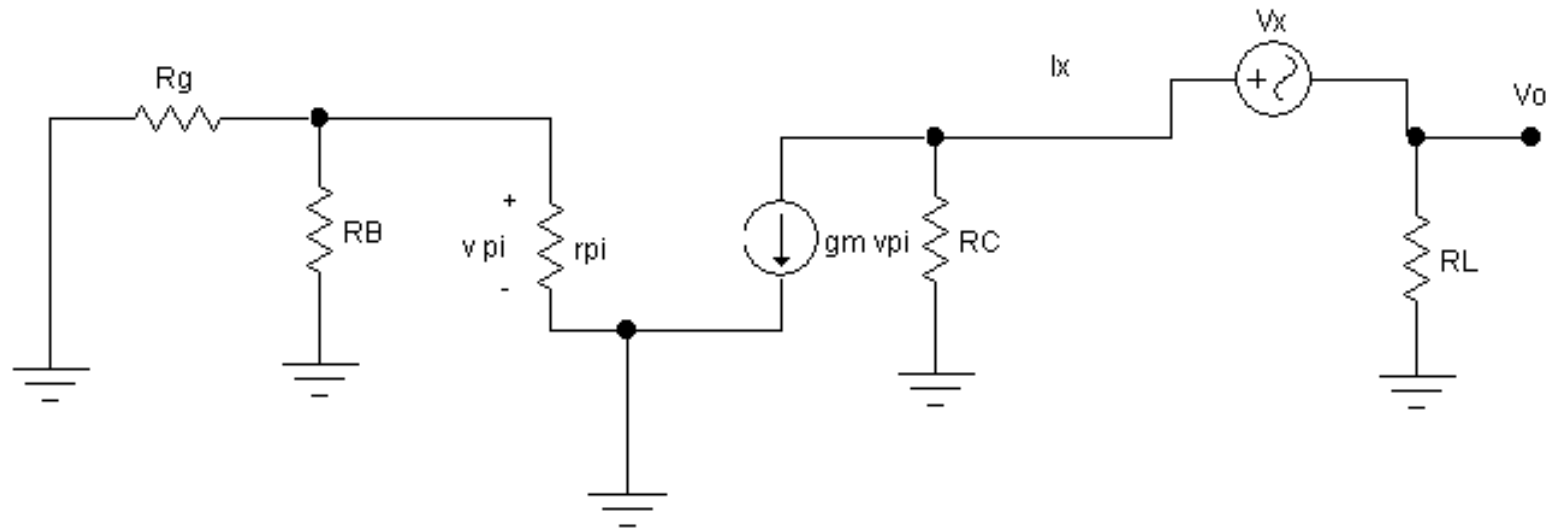
$$R_{Ci}^{\infty} = R_g + R_B // r_{\pi}$$

Short-circuit time constants method. EXAMPLE (III)



$$R_E^{\infty} = R_E \parallel \frac{r_{\pi} + (R_g \parallel R_B)}{1 + \beta_0}$$

Short-circuit time constants method. EXAMPLE (IV)



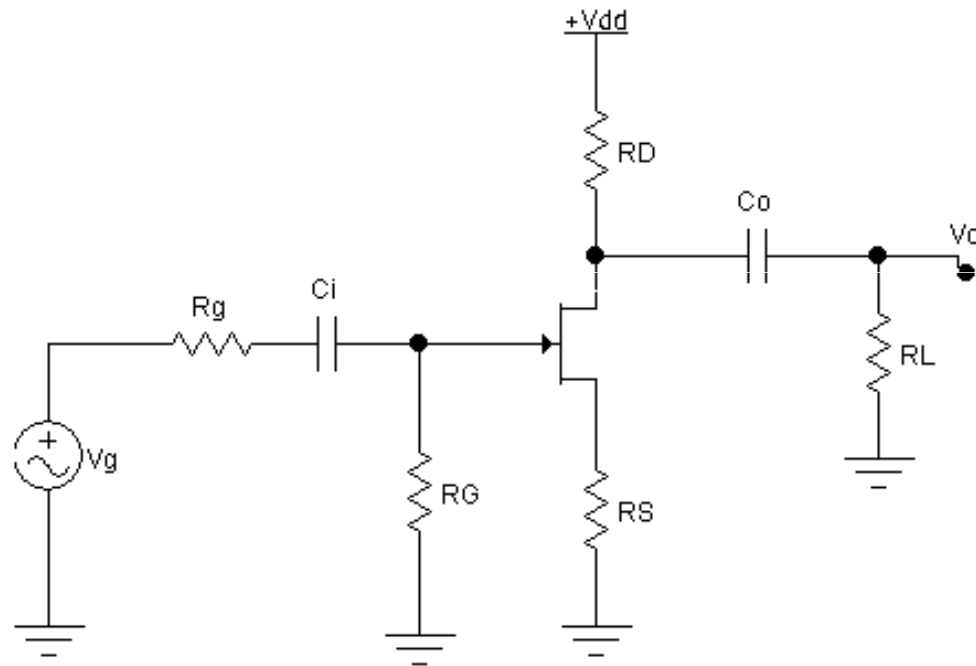
$$R_{C_o}^{\infty} = R_C + R_L$$

Short-circuit time constants method.

EXAMPLE (V)

$$f_{ci} = \frac{1}{2\pi} \left[\frac{1}{C_i(R_g + R_B // r_\pi)} + \frac{1}{C_E \left(R_E // \frac{r_\pi + (R_g // R_B)}{1 + \beta_0} \right)} + \frac{1}{C_o(R_C + R_L)} \right]$$

Proposed Exercise



$$+V_{DD} = 15 \text{ V}$$

$$R_S = 560 \Omega$$

$$R_G = 1 \text{ M}\Omega$$

$$R_g = 50 \Omega$$

$$R_D = 5,6 \text{ K}\Omega$$

$$R_L = 10 \text{ K}\Omega$$

$$C_i = 10 \mu\text{F}$$

$$C_o = 10 \mu\text{F}$$

Transistor:

$$I_{DSS} = 10 \text{ mA}$$

$$V_P = -2 \text{ V}$$

$$C_{gd} = 0.36 \text{ pF}$$

$$C_{gs} = 1 \text{ pF}$$

$$I_D = I_{DSS} \cdot (1 - V_{GS}/V_P)^2$$